

Combustion of Metal Powders for Power and Heat Generation in Space Missions

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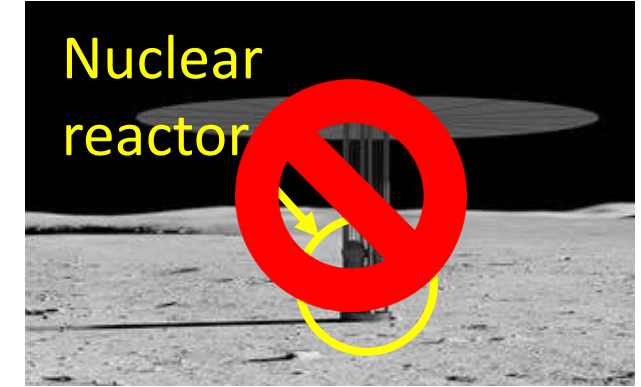
Space Power Systems



**Vertical solar array on the Moon
(under development)**



**Radioisotope thermoelectric generator (RTG)
of Curiosity rover**



**Conceptual nuclear power
system on the Moon**



Lithium-ion batteries for Sojourner rover

Combustion-based power system

- Specific energy and power are higher than for batteries.
- Unlimited energy storage time
- Especially advantageous if the lander or rover needs to be heated.

Power System Based on Li-SF₆ Combustion



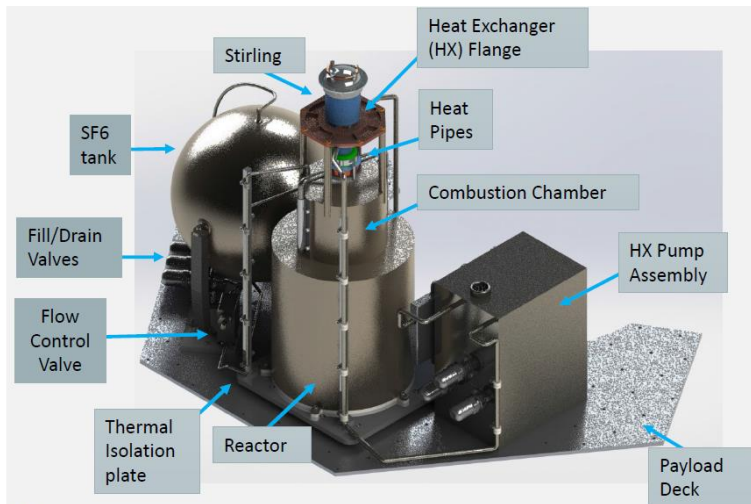
Li-SF₆ combustion has been used in the U.S. Navy's Mk-50 torpedoes.

- $8\text{Li} + \text{SF}_6 \rightarrow 6\text{LiF} + \text{Li}_2\text{S}$ 14.1 MJ/kg
- The condensed products occupy less volume than the used lithium.



Mk-50 torpedo being fired
Credit: U.S. Navy

Was recently under development at JPL for lunar night survival.



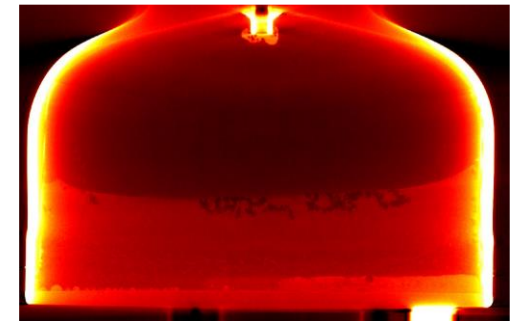
Li-SF₆ power system for lunar night survival



Reactor



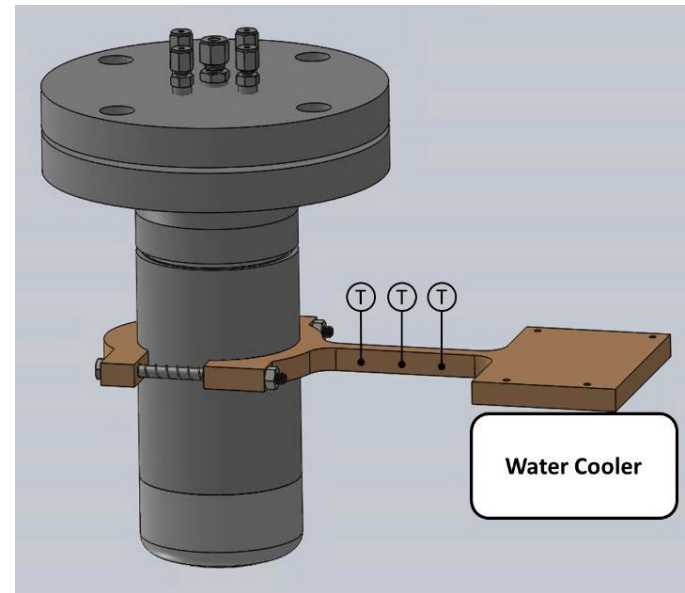
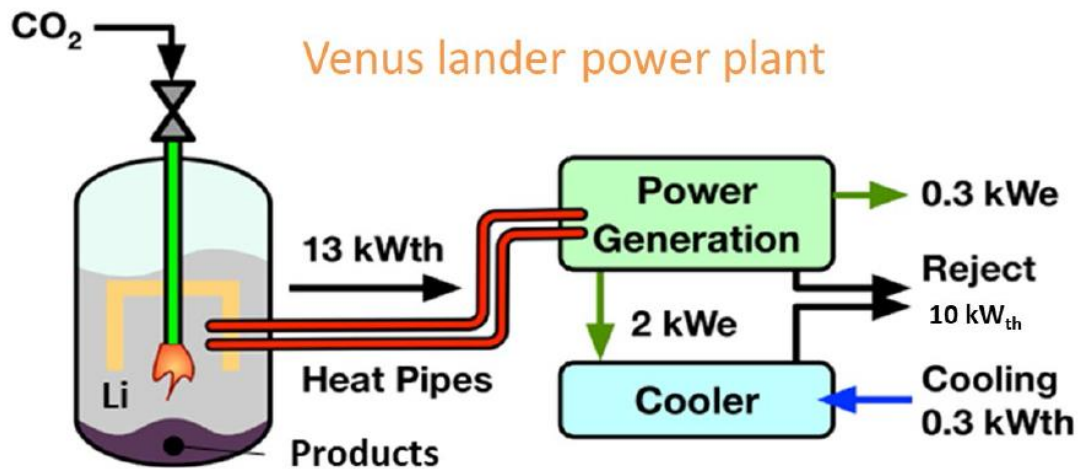
Cross-sectioning and CT scan of the reactor



Power System Based on Li-CO₂ Combustion

Was studied at Penn State – Applied Research Laboratory for cooling a Venus lander.

- Venus surface: 92 bar, 470 – 500 °C
- Li-CO₂ batch reactor combustion experiments



Schematic, photo, and CT scan of the reactor

Metal – O₂ Combustion?

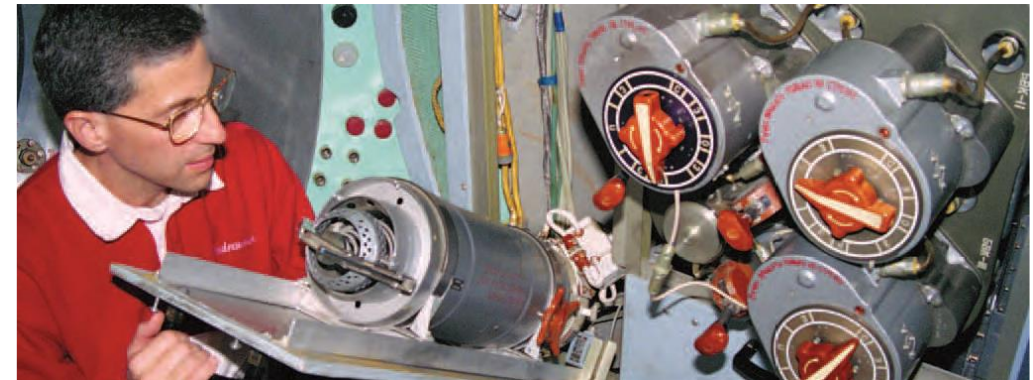


Energy per kilogram of the reactants



Chemical oxygen generator (“oxygen candle”)

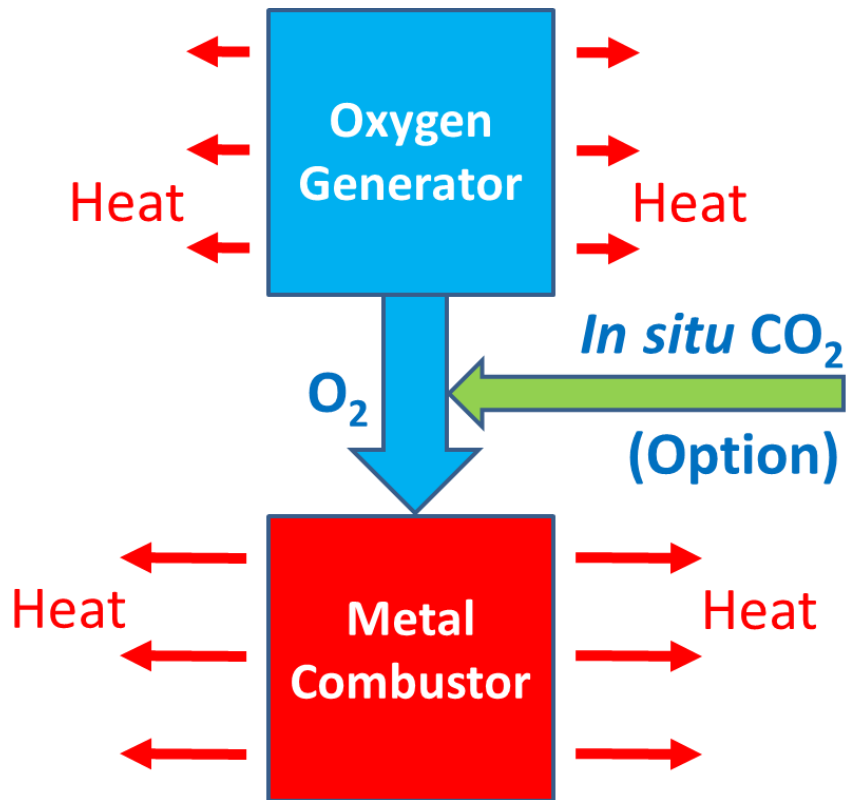
- Oxygen source: chlorates and perchlorates of Li or Na
- Widely used in aircraft, submarines, and space stations



A chemical oxygen generator for space stations

Image credit: NASA

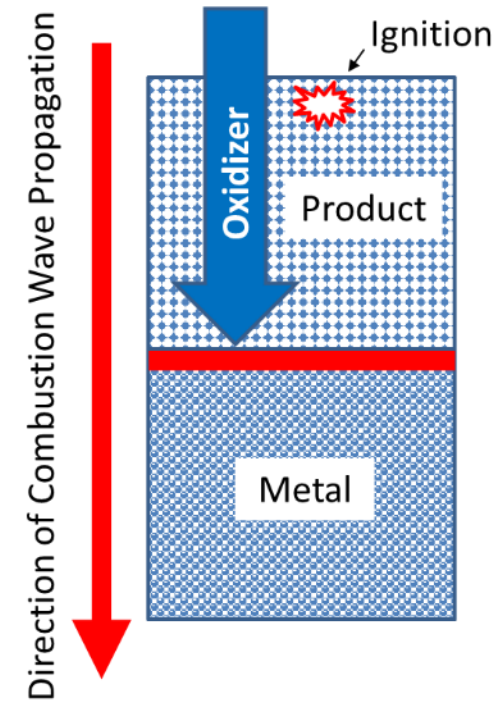
Metal-O₂ Power System



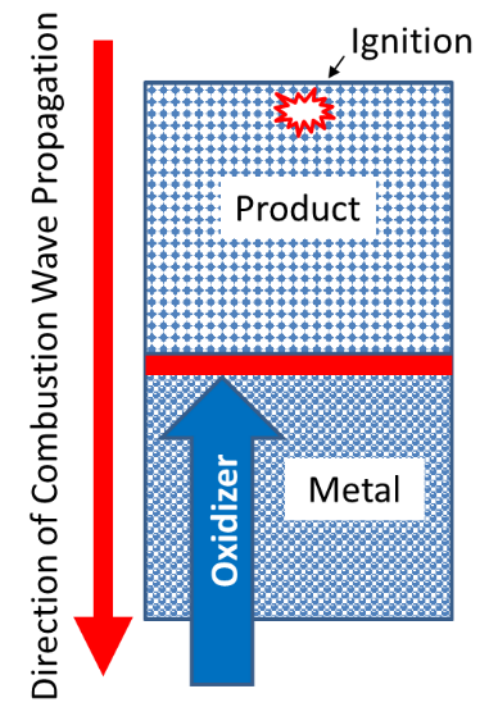
- The generated oxygen infiltrates through the metal powder to the reaction zone.
- Combustion is controlled by oxygen flow.
- Solid reactants and products
- Unlimited storage time
- Optional use of *in situ* CO₂ (Mars and Venus)

“Filtration Combustion” of Metal Powders

- Used for **combustion synthesis** of metal nitrides and hydrides.
 - Pressures **over 1000 bar** in the reactor to ensure enough gas in the reaction zone
- In space power systems, pressure must be much lower.
- Infiltration of the gaseous oxidizer due to pressure gradient is critical.



Coflow combustion



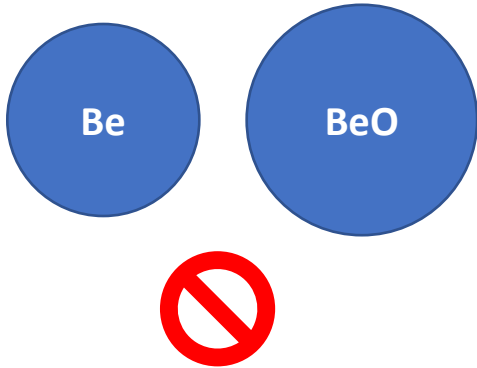
Counterflow combustion

Selection of Metal Fuel

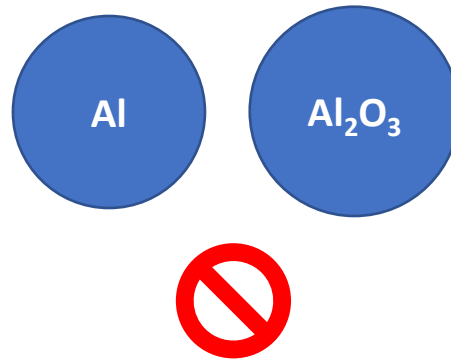
Pilling-Bedworth ratio: $R_{PB} = \frac{\text{Product volume}}{\text{Metal volume}}$

$R_{PB} < 1$ is desired.

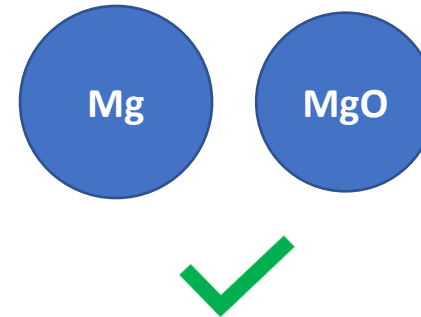
$$R_{PB} = 1.70$$



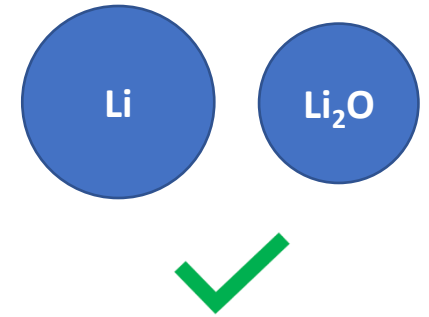
$$R_{PB} = 1.28$$



$$R_{PB} = 0.81$$



$$R_{PB} = 0.57$$



Li and Mg have been selected for further studies.

Mass Estimates for Lunar Night Survival



Li – SF₆ (JPL design)

SF₆ tank

- 15.84 kg, including 11.94 kg SF₆ (liquid at 22 bar and 294 K)

Mass of metal fuel

- 4.58 kg Li

Heat release

- 157 MJ

$$\frac{157}{15.84 + 4.58} = 7.7 \frac{\text{MJ}}{\text{kg}}$$

Metal – oxygen generator

Multi-purpose oxygen generator (MPOG, Molecular Products, 2600 L of O₂ at NPT)

- 12 kg, including 3.46 kg of oxygen

Mass of metal fuel

- 3.00 kg Li or 5.25 kg Mg

Heat release

- 132 MJ

$$\text{Li: } \frac{132}{12 + 3.00} = 8.8 \frac{\text{MJ}}{\text{kg}}$$

$$\text{Mg: } \frac{132}{12 + 5.25} = 7.7 \frac{\text{MJ}}{\text{kg}}$$

Note: Mg is 3.25 times denser than Li.

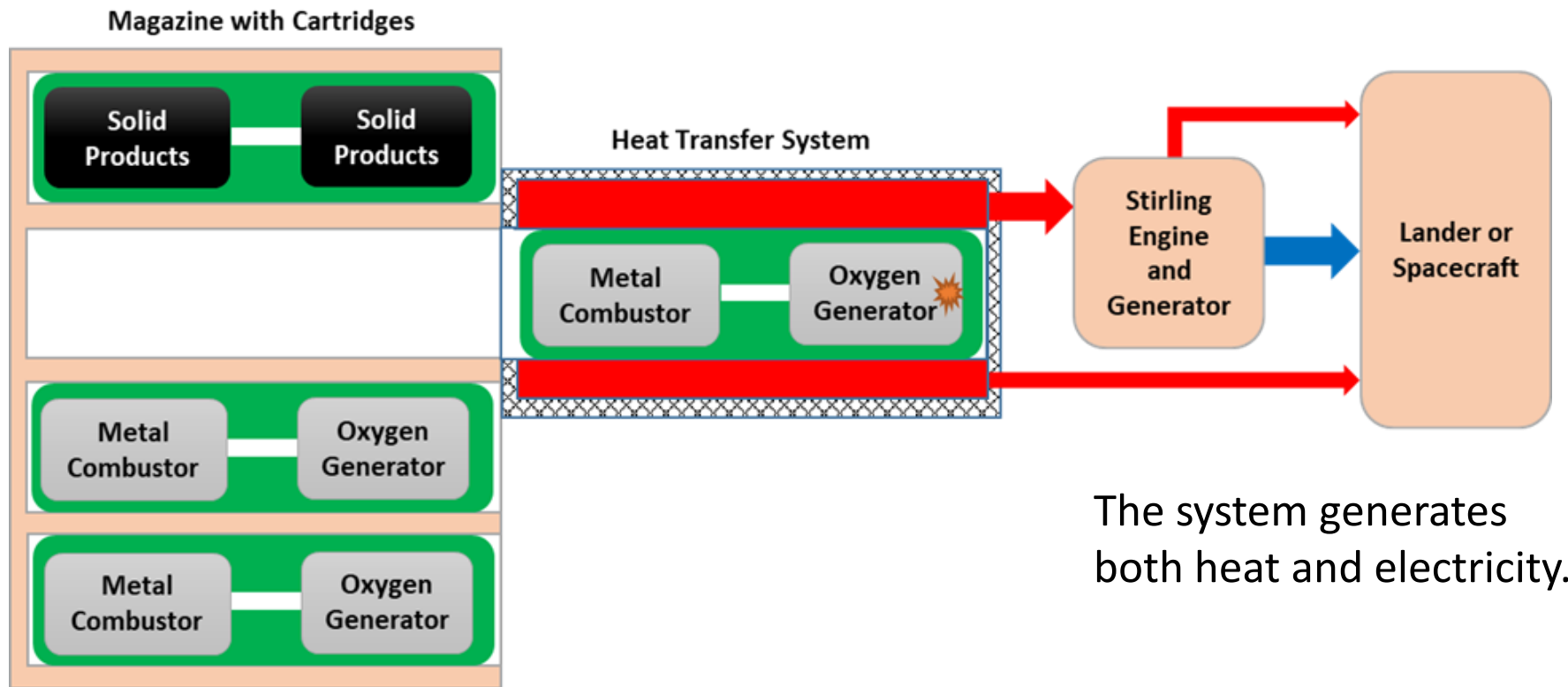


MPOG

Credit: Molecular Products

Multiple Heat-generating Cartridges

Could be used in a long mission, such as the lunar night survival.



The system generates both heat and electricity.

Power system with cartridges

Mass Estimates for Design with Cartridges



Lunar night survival mission, 14 days, total energy: 157 MJ (44 kWh)

- Li – SF₆ (JPL design)
- Li – COGs for aircraft
- Mg – COGs for aircraft



COGs for aircraft

Credit: B/E Aerospace

	Li – SF ₆	Li - COGs	Mg - COGs
Mass of SF ₆ tank, kg	15.84	-	-
O ₂ capacity of COG, L	-	80	80
Mass of COG, kg	-	0.45	0.45
Number of cartridges	-	40	40
Mass of all COGs, kg	-	18	18
Mass of fuel, kg	4.58	3.69	6.46

The masses of all COGs and Li or Mg are comparable with those of SF₆ tank and Li.

1. Kinetics and mechanisms of Mg and Li reactions with O_2 and CO_2

- Thermoanalytical methods (TGA and DSC)

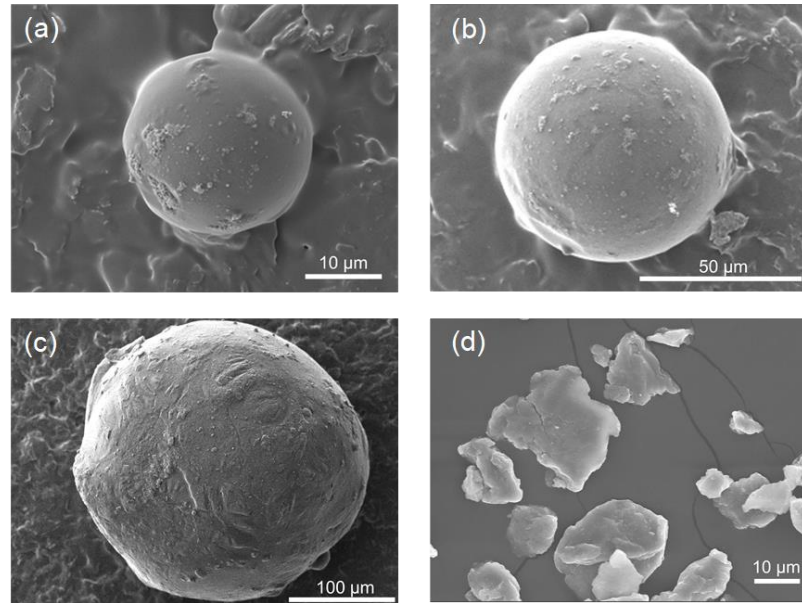
2. Combustion of Mg and Li powders with infiltrating O_2 and CO_2

- Closed chamber; pressure difference due to consumption of the oxidizer → natural infiltration
- If the combustion at natural infiltration is possible, combustion at forced infiltration is expected.

Mg and Li Powders

Spherical Mg particles

- $d_{50} = 32\text{ }\mu\text{m}$ (Mg30)
- $d_{50} = 57\text{ }\mu\text{m}$ (Mg60)
- $d_{50} = 282\text{ }\mu\text{m}$ (Mg300)



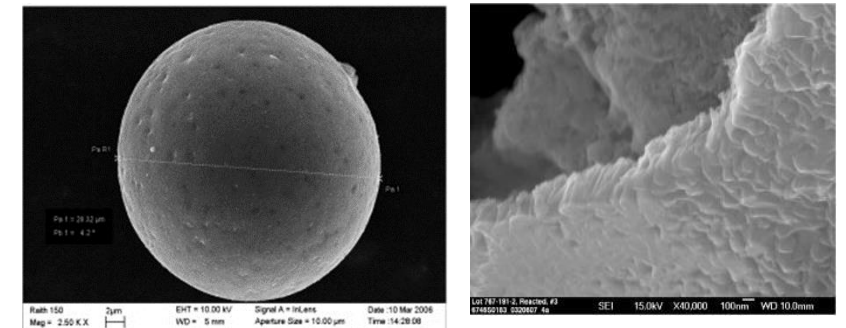
SEM images of Mg particles

Mg flakes

- $d_{50} = 28\text{ }\mu\text{m}$

Stabilized lithium metal powder (SLMP®)

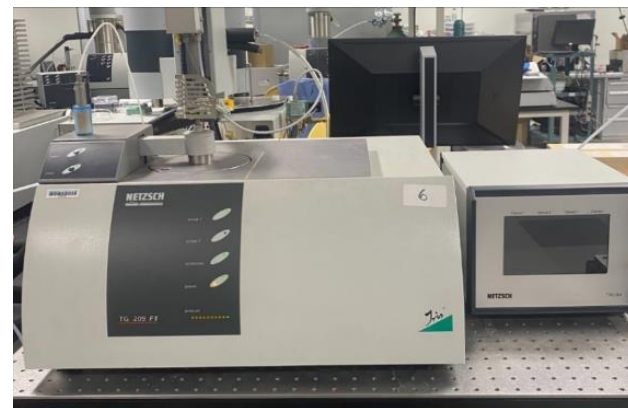
- Non-pyrophoric in dry air due to Li_2CO_3 coating.
- $d_{50} = 50\text{ }\mu\text{m}$



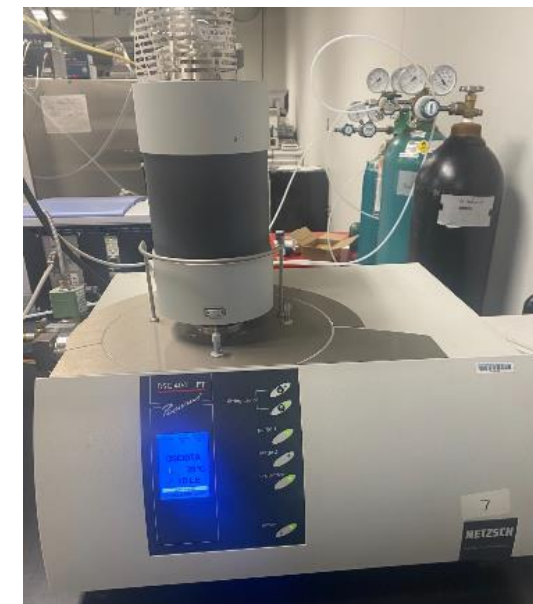
SEM images of an SLMP particle and a broken edge of the coating on a reacted SLMP particle

Thermoanalytical Studies

- **Thermogravimetric analysis (TGA) and differential scanning calorimetry (DSC)**
 - Sample: 0.5-1.0 mg
 - Gas environments: O₂, O₂/Ar, CO₂
 - Non-isothermal tests
 - Heating rates: 1 – 10 K/min
 - Isothermal tests
 - Temperatures: 300 – 575 °C
- **Scanning electron microscopy (SEM)**
- **X-ray diffraction analysis (XRD)**

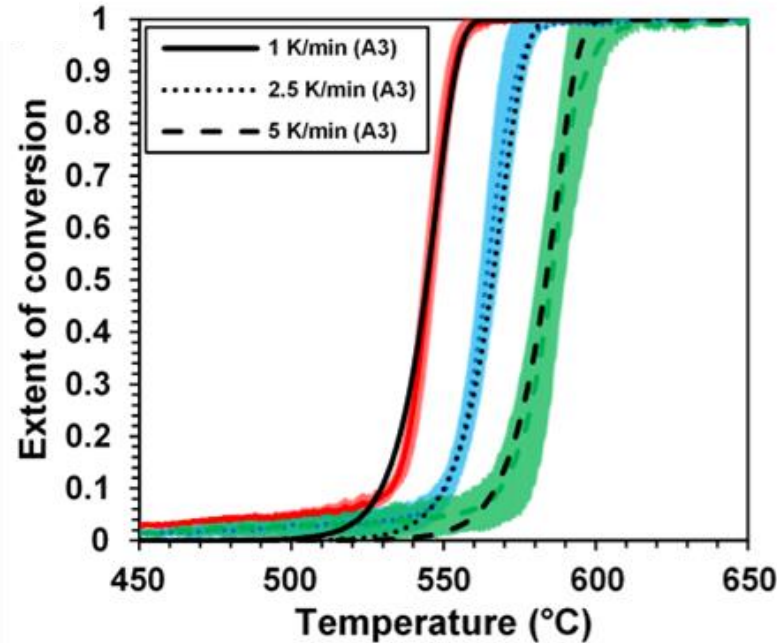


Netzsch TG 209 F1 Iris



Netzsch DSC 404 F1 Pegasus

Non-isothermal TGA of Mg in O₂



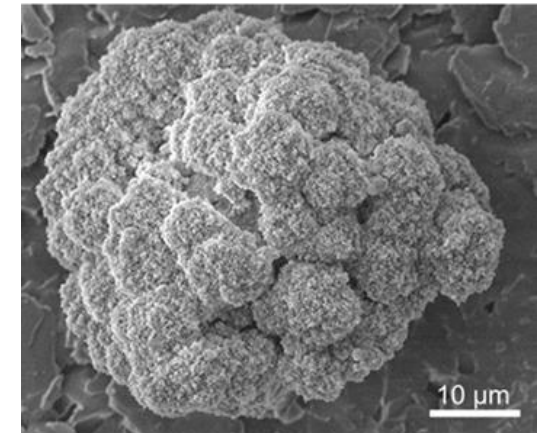
TGA curves for Mg30 fitted to the Avrami-Erofeev model

- Oxidation is complete **before melting** of Mg (650 °C).
- The Avrami-Erofeev model (both **nucleation** and **growth** occur in the bulk) provides the best fit with the TGA curves.

$$\frac{d\alpha}{dt} = A \exp\left(-\frac{E}{RT}\right) f(\alpha)$$

$$f(\alpha) = n(1 - \alpha)[- \ln(1 - \alpha)]^{(n-1)/n}$$

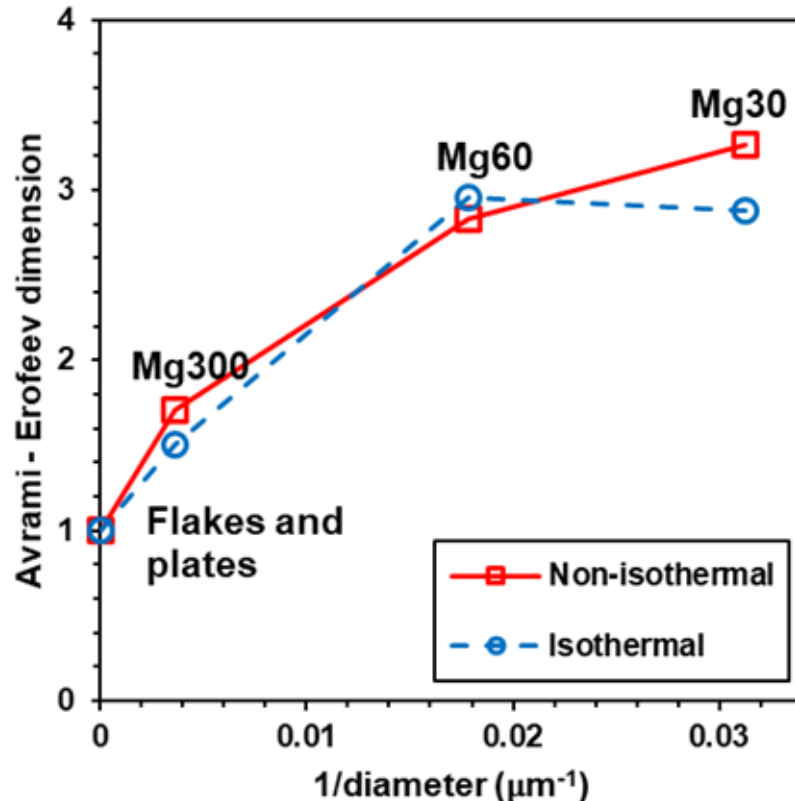
- Apparent activation energy:
200 – 230 kJ/mol
- Submicron grains are consistent with the Avrami-Erofeev model.



SEM image of Mg30 particle after oxidation

Isothermal TGA of Mg in O₂

$$f(\alpha) = n(1 - \alpha)[- \ln(1 - \alpha)]^{(n-1)/n}$$



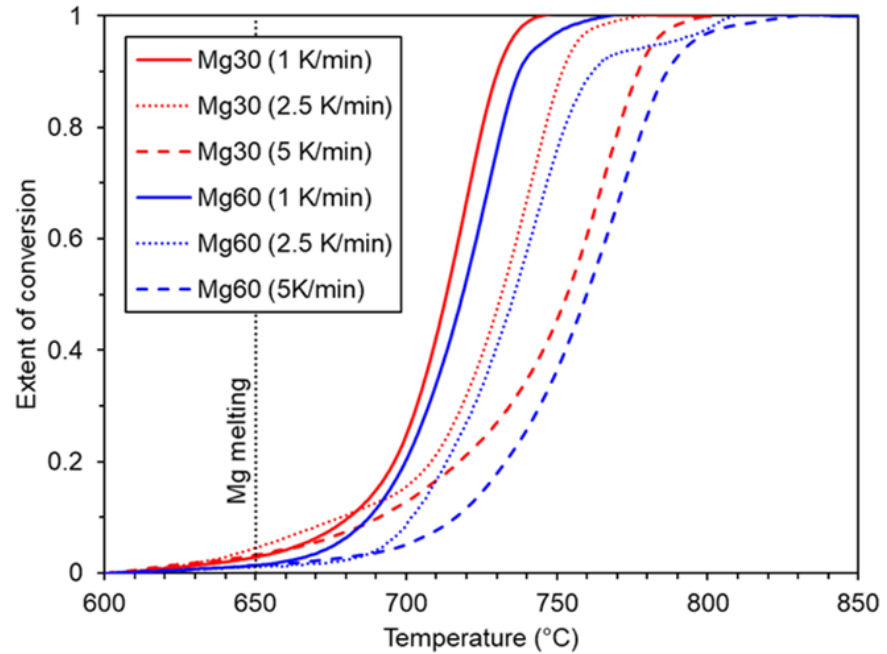
The dimension n of the Avrami-Erofeev equation vs. the reciprocal of the diameter

- The dimension n of the Avrami-Erofeev equation decreases with decreasing the curvature.

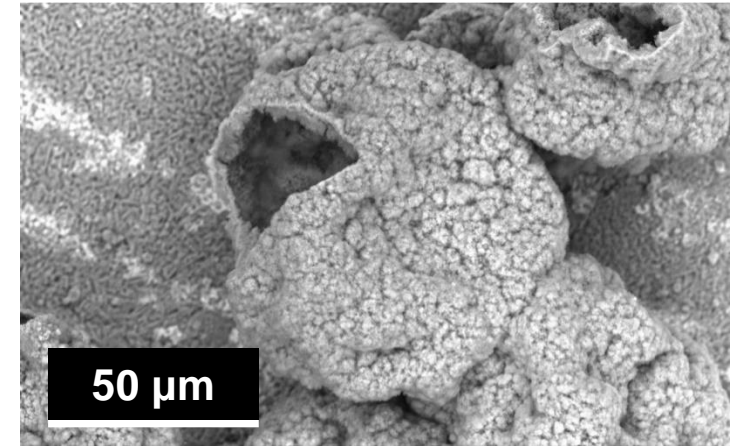
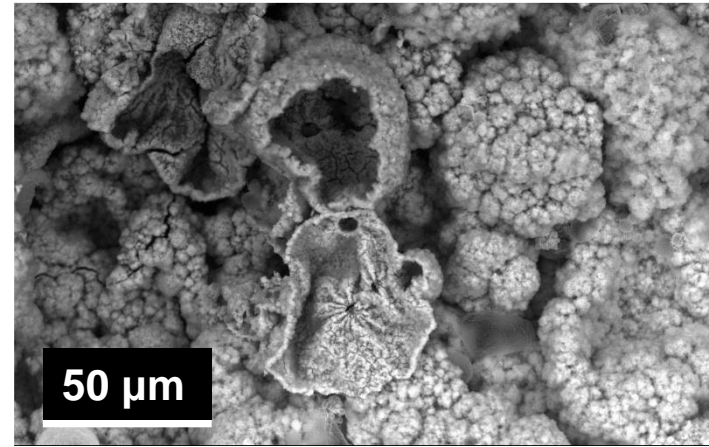
Mampel-Delmon analysis of the isothermal TGA data

- Nucleation on the surface and isotropic growth inward.
- Small (30 – 60 μm) spherical particles: slow nucleation.
 - $n = 3$
- With increasing size (300 μm), nucleation is faster, and its effect on the overall kinetics is smaller.
 - $n < 2$
- Flakes and plates: The overall kinetics is determined by the growth of a non-protective oxide layer.
 - $n = 1$ $f(\alpha) = 1 - \alpha$ – linear oxidation law

Non-isothermal TGA of Mg in CO₂



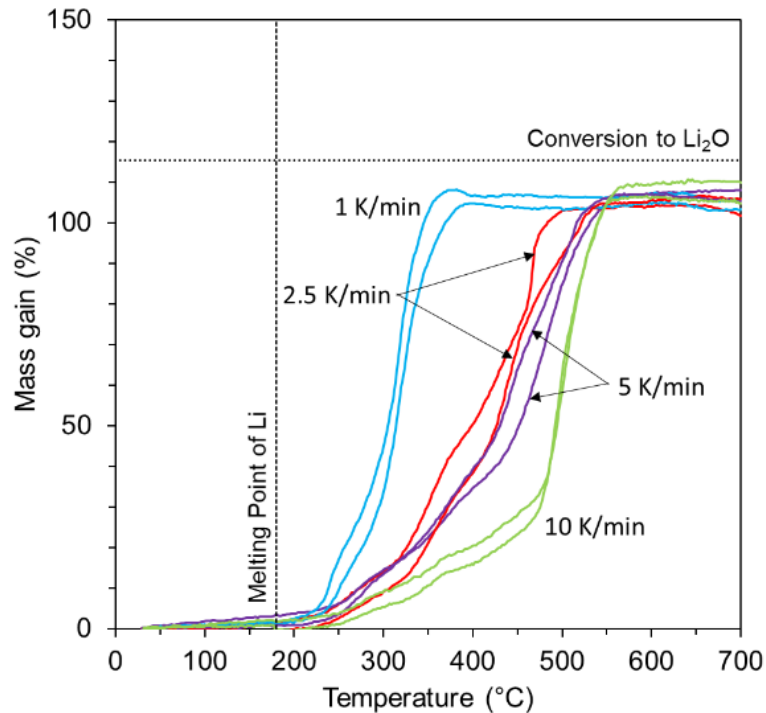
TGA of Mg particles in CO₂



SEM images of Mg30 (left) and Mg60 (right) particles after reaction with CO₂

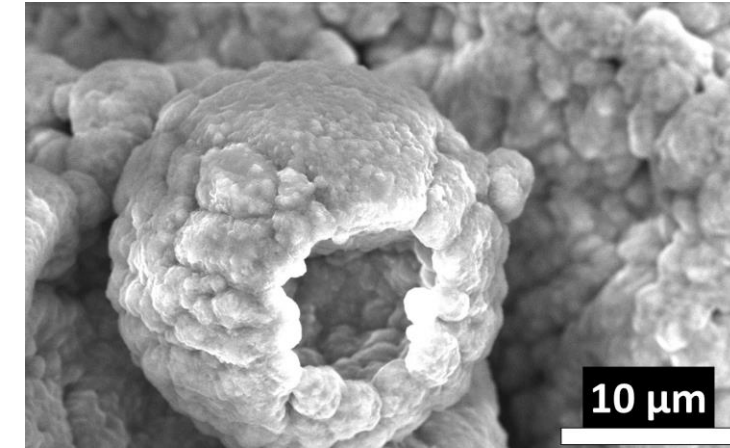
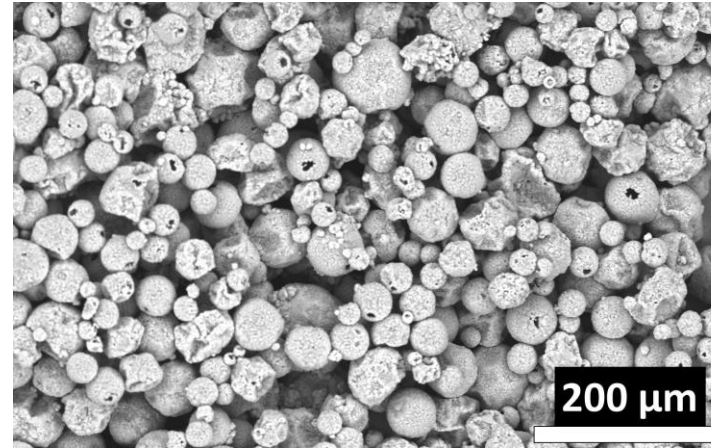
- **Hollow spheres:** Molten Mg spreads **outward** through the pores and reacts with CO₂ on the outer surface.
- Significant conversion only **after melting**

Non-isothermal TGA of Li in O₂/Ar



TGA of Li particles in O₂/Ar (10% O₂)

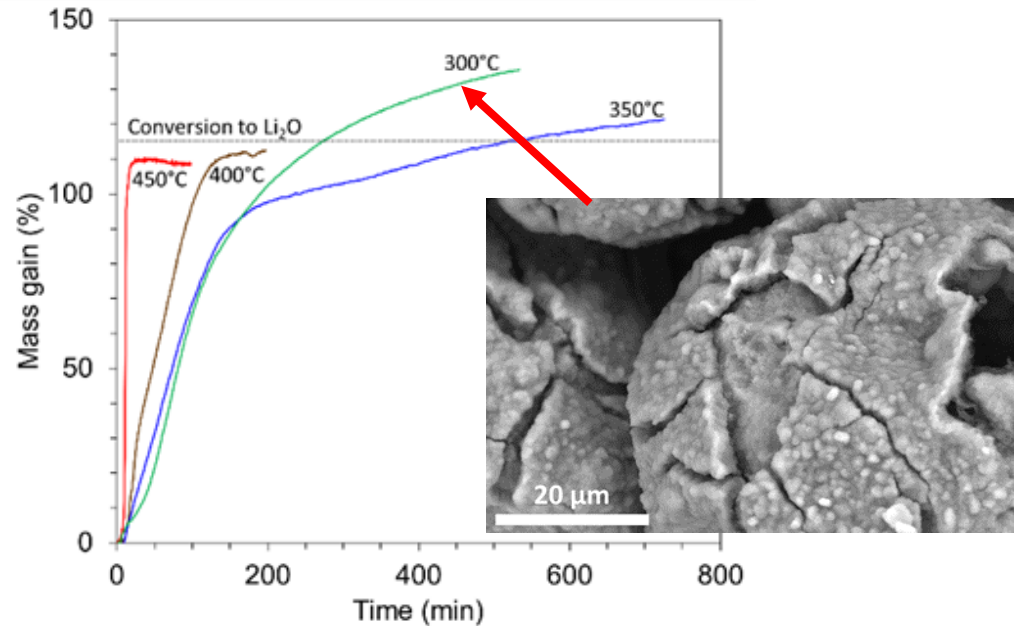
- Mass gain is close to 115% – oxidation of Li to Li₂O.
- Reaction occurs **after melting** of Li.
- Transition to a faster second stage



SEM images of Li particles after oxidation

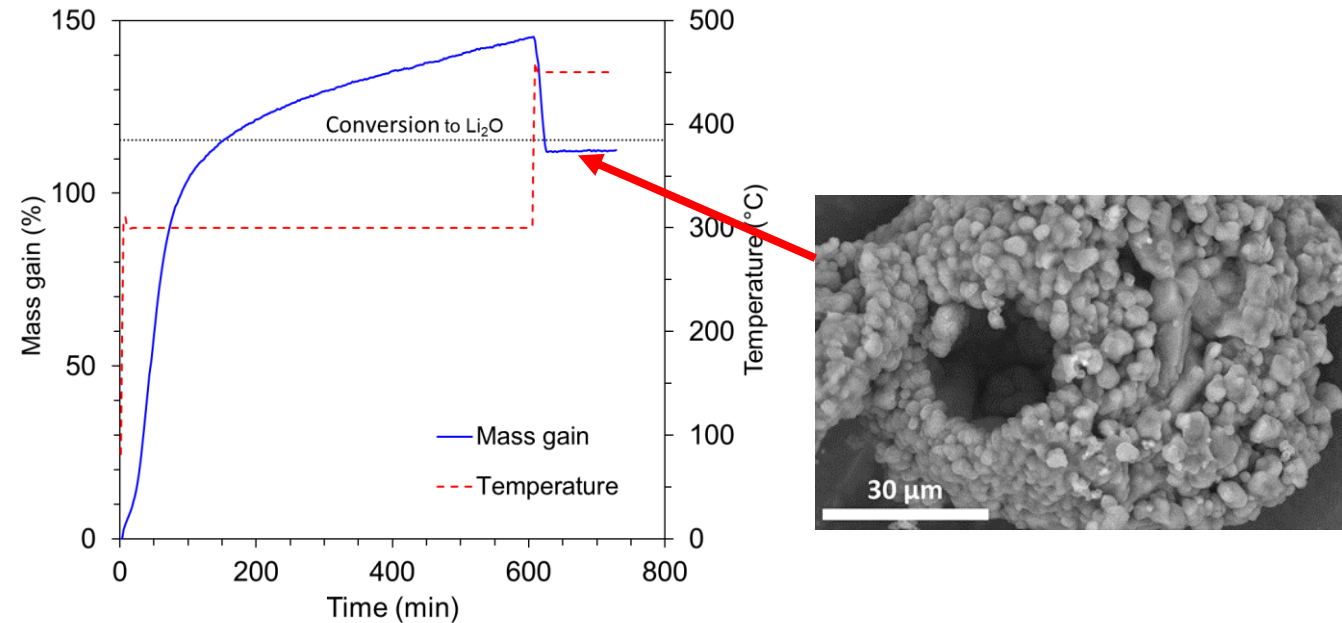
- **Hollow spheres:** Molten Li spreads **outward** through the pores and reacts with O₂ on the outer surface.

Isothermal Oxidation of Li in O₂/Ar



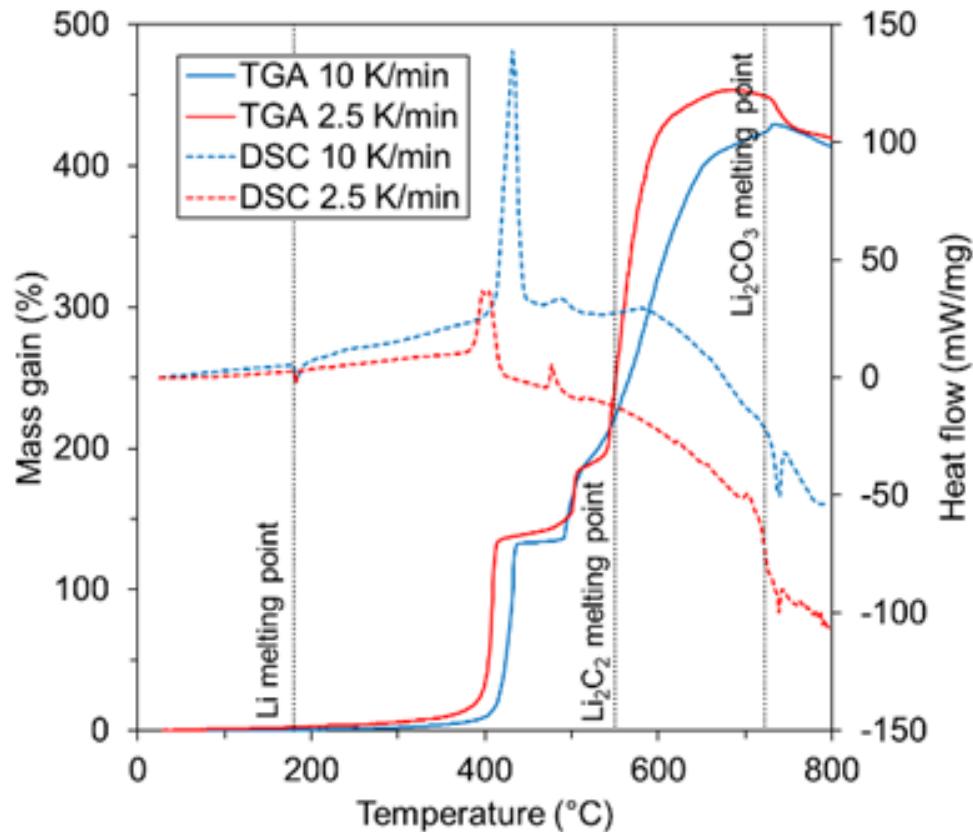
TGA of Li particles in O₂/Ar (10% O₂)

- At 300 and 350 °C, the mass gain indicates **formation of Li₂O₂** along with Li₂O.
- At 400 and 450 °C, only Li₂O forms.
 - Li₂O₂ decomposes.



- Test to confirm formation and decomposition of Li₂O₂
 - After 600 min of heating at 300 °C, the temperature was raised to 450 °C.
 - The mass dropped to about 115%.
- **Decomposition of Li₂O₂ explains the transition to a faster reaction in the non-isothermal TGA tests.**

Non-isothermal TGA of Li in CO₂

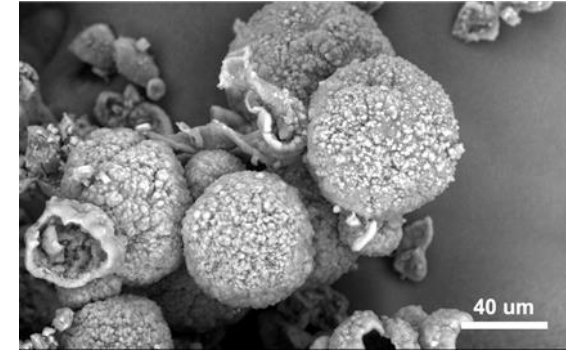


TGA and DSC of Li particles in CO₂

- Reaction starts **after melting** of Li.

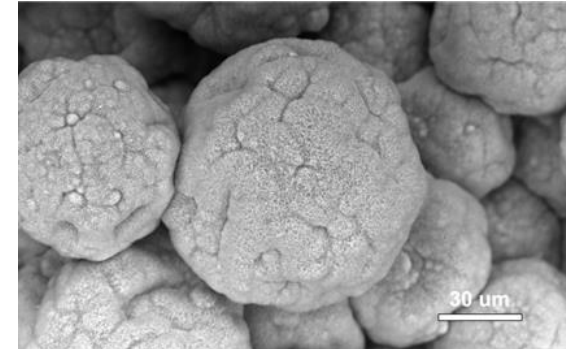
1. Formation of Li₂O

- At about 400 °C
- $2\text{Li} + \text{CO}_2 \rightarrow \text{Li}_2\text{O} + \text{CO}$
- $4\text{Li} + \text{CO}_2 \rightarrow 2\text{Li}_2\text{O} + \text{C}$

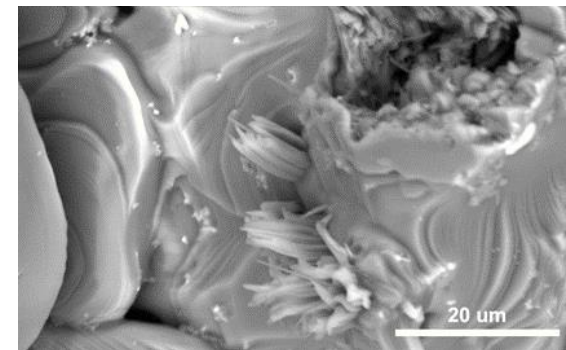


2. Formation of Li₂CO₃

- At 500 – 700 °C
- $\text{Li}_2\text{O} + \text{CO}_2 \rightarrow \text{Li}_2\text{CO}_3$

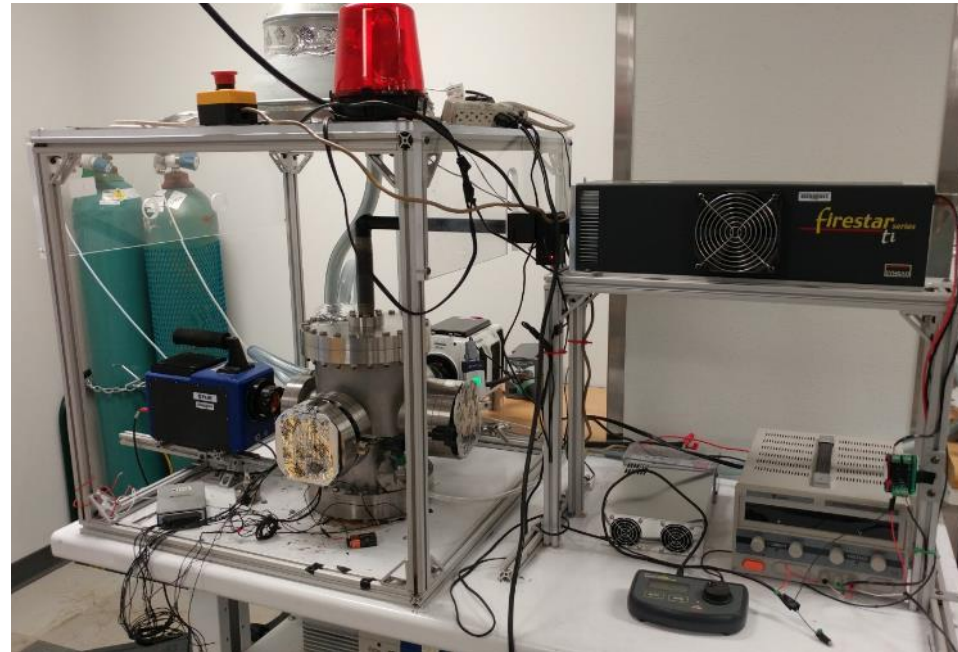


3. Melting and decomposition of Li₂CO₃

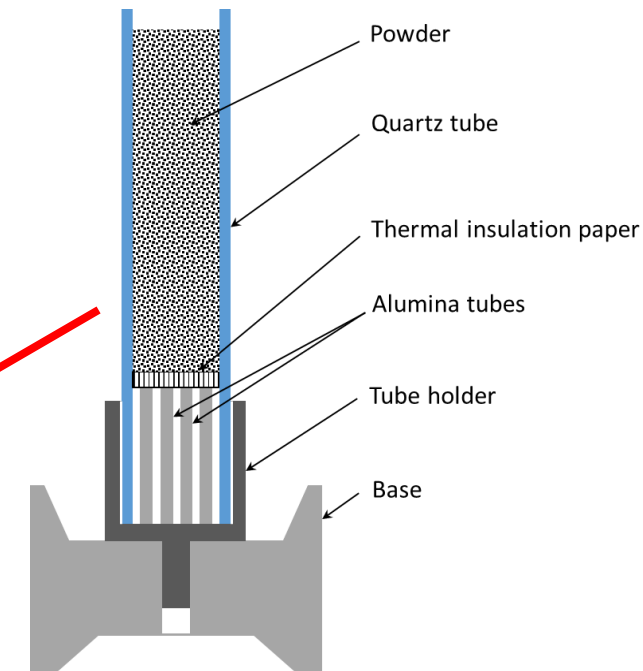
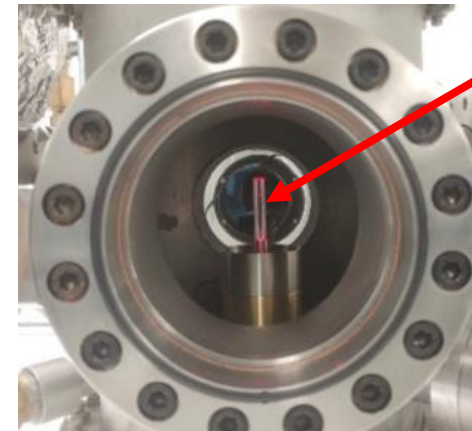


Combustion Experiments

- **Windowed vacuum chamber**
- **Metal powder in a quartz tube**
 - ID: 2-7 mm
 - Gas infiltrates from both ends.
- **Environments: O₂ and CO₂**
 - Pressure: 13 – 90 kPa
- **Laser ignition at the top**
- **Diagnostics**
 - High-speed video recording
 - Infrared video recording
 - Thermocouple measurements
 - Analysis of products



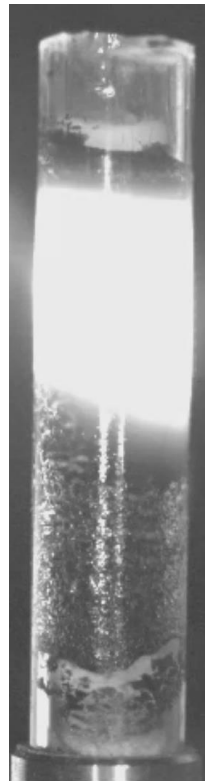
Laser ignition setup



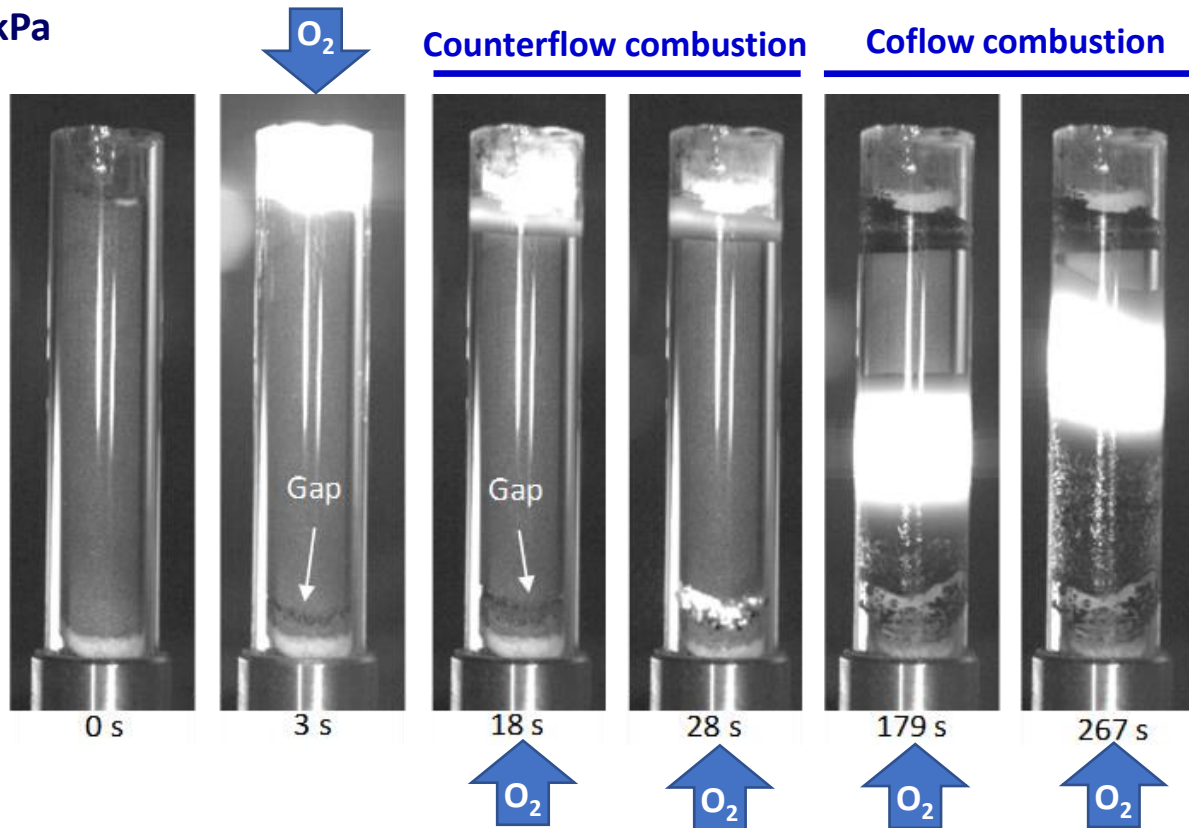
Quartz tube with sample

Combustion of Mg Powder in O₂

ID = 7 mm, P = 90 kPa

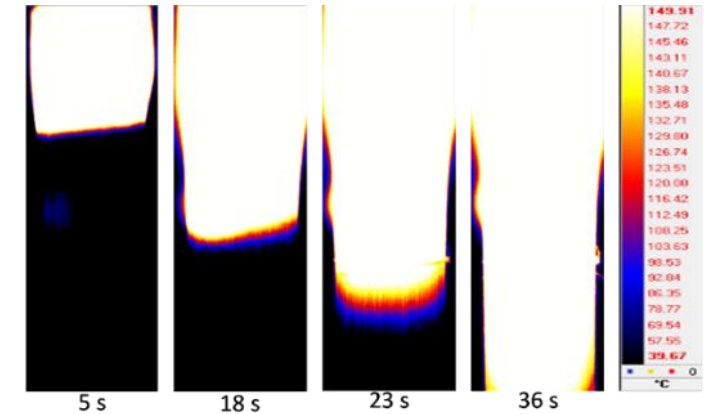


Video plays
at 5x speed

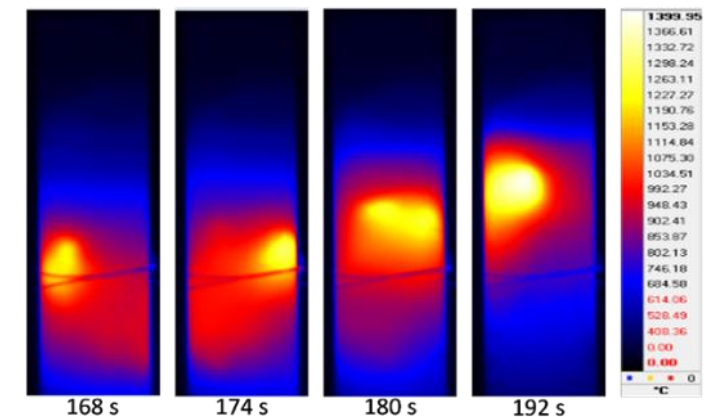


1. Ignition at the top, formation of a gap at the bottom
2. Downward propagation of a counterflow combustion wave
3. Upward propagation of a coflow combustion wave

Wave down

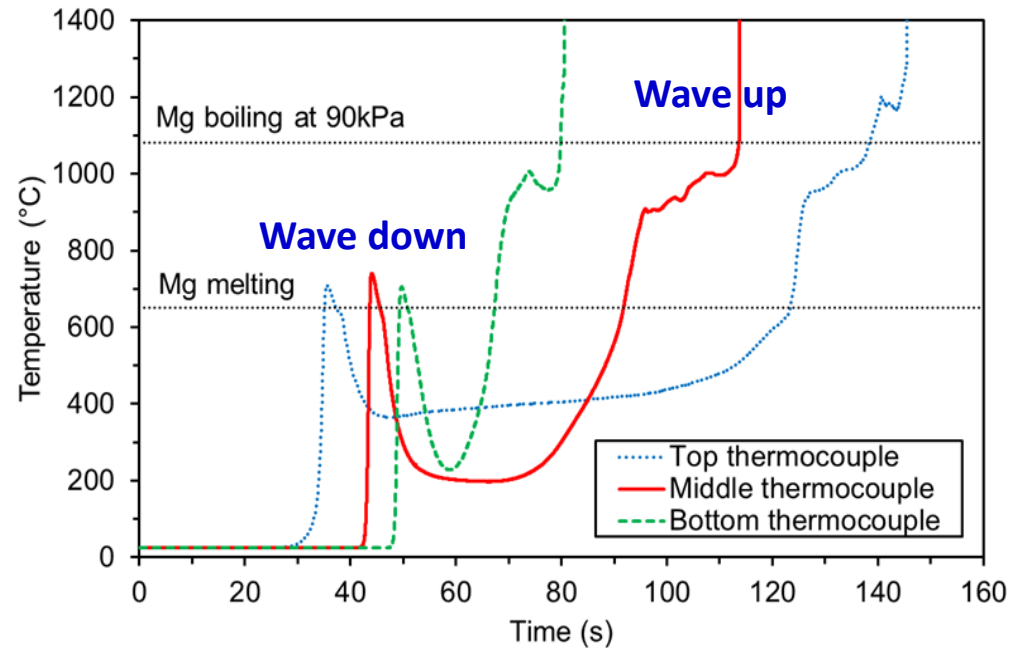


Wave up



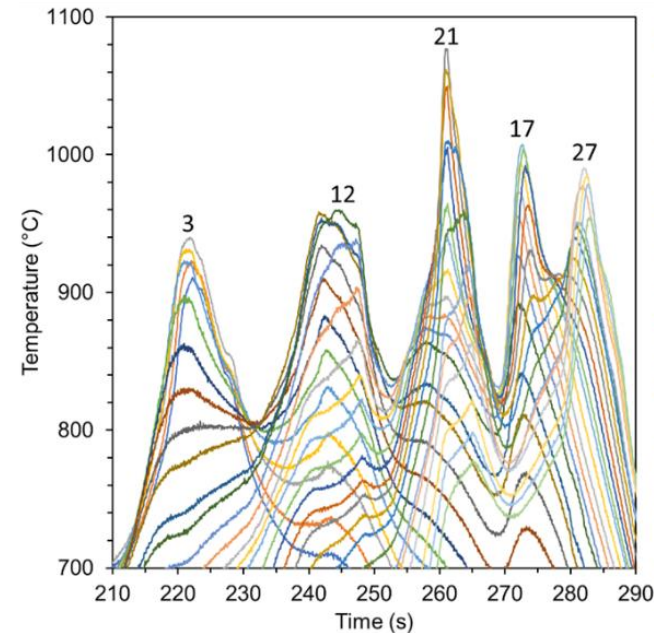
Infrared video recording

Combustion of Mg Powder in O₂, Cnt'd



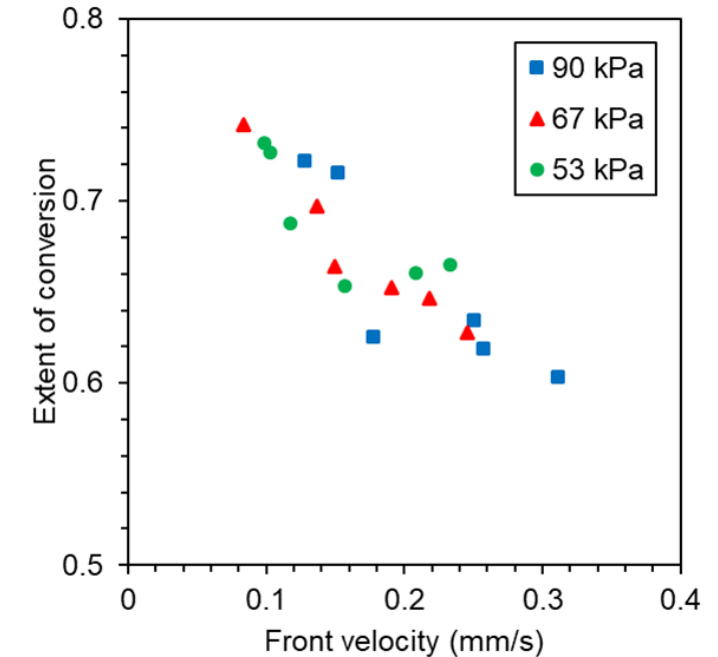
Thermocouple measurements confirm two combustion waves

1. Wave down
2. Wave up



Analysis of infrared video images for the upward wave

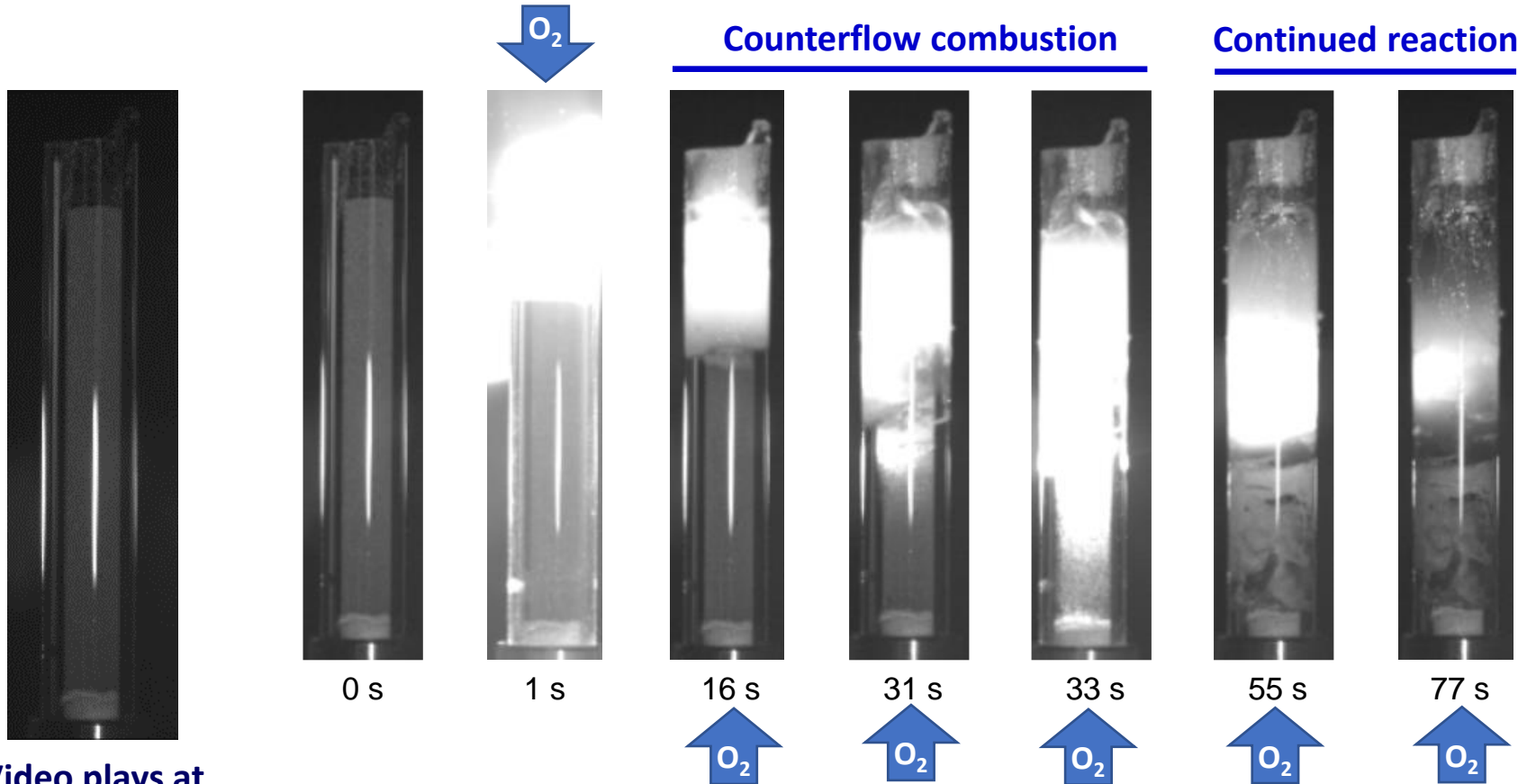
- Spinning propagation



- Lower front velocity increases conversion.
- Front velocity: 0.1 – 0.3 mm/s

Combustion of Li Powder in O₂

ID = 4 mm, P = 90 kPa



1. Ignition forms an impermeable product layer.
2. A thermal wave propagates downward (**0.2 – 0.3 mm/s**), while oxygen infiltrates from the bottom.
3. Reaction continues over the entire sample.

Video plays at
actual speed

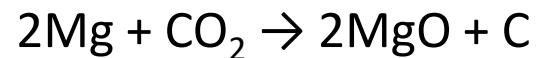
Combustion of Mg and Li Powders in CO₂



Self-sustained propagation of the combustion wave was not achieved in CO₂.

Transport of CO₂ could be hindered by:

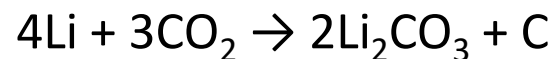
- A protective product layer (MgO/C and Li₂CO₃/C) on the particle surface
- CO in the pores between the particles



$$R_{pB} = 1.02 - \text{protective}$$



$$R_{pB} = 0.81 - \text{non-protective, CO forms}$$



$$R_{pB} = 1.45 - \text{protective}$$



$$R_{pB} = 1.35 - \text{protective, CO forms}$$

Conceptual design of a power system based on combustion of metal powders

- The use of Li and Mg fuels with chemical oxygen generators for heat and power production during lunar night is competitive with Li-SF₆ combustion.

High-temperature oxidation of Mg and Li powders

- Oxidation of Mg particles in O₂ is well described by the Avrami-Erofeev equation, while the Mampel-Delmon analysis shows how that the dependency of the model parameters on the particle size is related to the rates of nucleation and growth.
- Oxidation of Li particles by O₂ involves formation and then decomposition of Li₂O₂.
- Reaction of Li with CO₂ first produces Li₂O, which is then converted into Li₂CO₃.

Combustion of Mg and Li powders with infiltrating oxygen

- Ignition results in a counterflow combustion wave at incomplete conversion, followed by a backward coflow wave or by a reaction over the entire sample.

Thank you!

