

# Orion CFD Analysis

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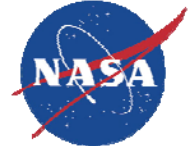
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# Outline

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- **CEV (Orion) Aeroscience Project (CAP) Computational overview**
- **Challenges/issues in Orion CFD analysis**
  - Crew Module (CM)
  - Launch Abort Vehicle (LAV)
- **Final thoughts**



# CAP Computational Overview

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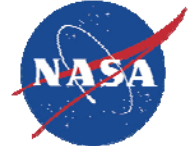
**Initial Orion planning was to develop the aero/aerothermal databases using only CFD to reduce costs.**

- CAP believes WTT is needed to compliment CFD analysis, and has developed the databases using CFD and testing.
- First cut estimate of planned CFD analysis required ~11 million cpu-hrs
  - Case matrix not intended to cover more than one iteration of the database (frozen design).
  - CAP lacked full understanding of the complexity of the LAV parameter space
  - Estimate was success oriented based on original design similarity to Apollo
- To date, CAP has used ~28 million cpu-hrs – 11 for aerothermal, ~17 aero
  - Orion design has changed/evolved several iterations (not unexpected)
    - Multiple OML changes/re-designs, LAV motor changes, etc.
  - Computational grids required for accurate modeling are larger than original estimates.
  - Several analyses have required case duplication to assess sensitivity to modeling limitations.
  - + Current database has large WTT contribution.
    - CFD derived WTT-to-flight corrections for several database segments.

**Completed work has focused on Launch Abort Vehicle (LAV) characterization for ascent-abort flight tests.**

**Current work is focused on analysis supporting EFT-1 – mostly detailed Crew Module (CM) aerodynamics, RCS effects, ...**

# Orion Aero CFD Challenges/Issues



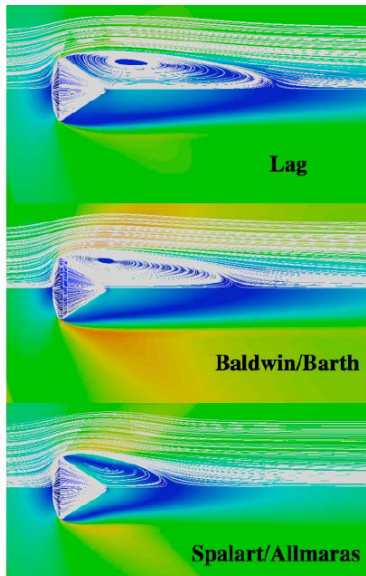
**CFD for configurations with separated flows and/or shear layers that drive aerodynamics is not at “database production” maturity level.**

- Separation/shear layer flows have been responsible for the vast majority of the issues CAP has encountered.
  - **CM entry** – bluff body separated flow prediction influences subsonic drag and pitching moment.
    - CFD predicted drag at subsonic conditions was lower than WTT – resulting uncertainty drove parachute deploy conditions to be more severe.
  - **CM forward bay cover jettison** – 2 body separation aerodynamics within the CM wake flow.
    - Jettison system performance is insufficient to tolerate current (necessarily) large aero uncertainty in combination with other system dispersions.
    - Defining this highly dynamic aerodynamic environment is challenging.
  - **Jet interactions** (ACM, AM/ACM, AM, CM RCS, LAT jettison)
    - Orion's LAV configuration and high abort dynamic pressure result in highly non-linear aero with large sensitivity to small plume changes.
    - Plumes are sensitive to the turbulence/shear layer modeling (esp. when inclined to the flow).
    - Shear layer physics differ between cold gas WTT and flight plumes.
    - Turbulence models tuned for shear layers may not perform well for wall bounded flows and vice versa.

# CM CFD issues

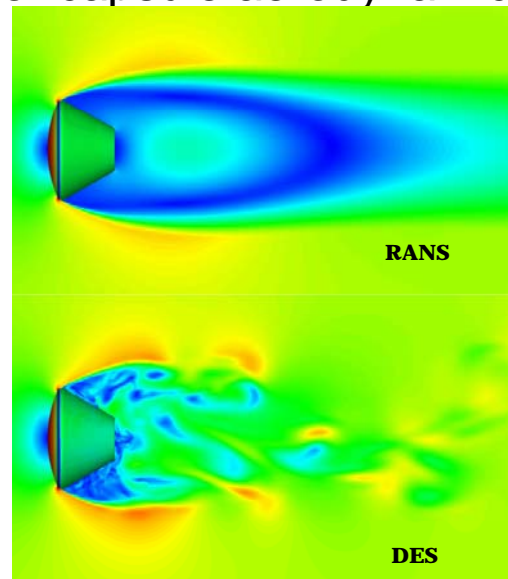
## Turbulence modeling for bluff bodies/wake flows

- Available turbulence models are generally tuned for wall-bounded flows.
- CFD analysis of Apollo config during Phase 1 showed large variations of aerodynamics with different turbulence models.
- Apollo WTT data also showed a considerable spread depending on facility/Re#
  - Lead to difficulty in determining the best performing turbulence model(s).
- “Best practices” development effort evaluated turbulence/grid resolution/numerical schemes for capsule aerodynamics.



Img : Neal Chaderjian

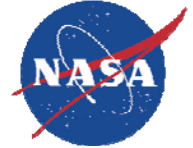
- Turbulence models predict widely different wake structures. Lag & Baldwin-Barth predicts long “long/thin” wakes – SA predicts “short/fat” wake and higher drag.
- Performance varied with AOA/Mach
- SST selected as best performer overall.



Img : Scott Murman

- RANS solutions tend to predict large scale coherent steady vortex structure near 180 deg alpha.
- DES has completely different wake structure, but integrated aerodynamic coefficients (time-averaged) tend to be relatively close, while wake environments ( FBC or parachutes) are not.

# CM CFD recommendations



## Grid :

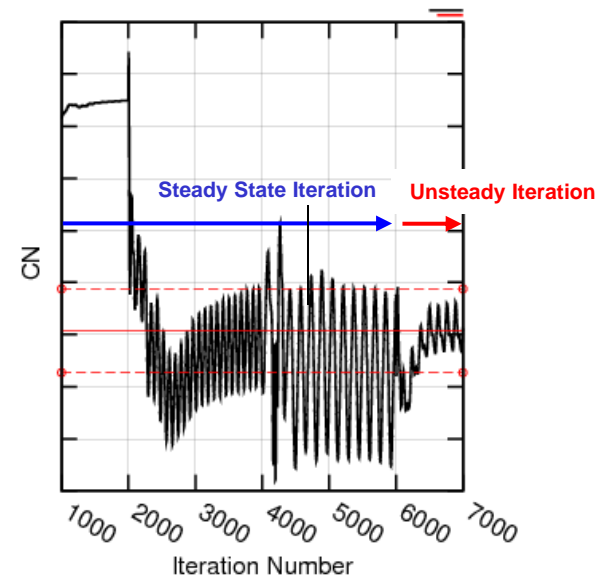
- Ensure grid convergence when performing sensitivity analyses.
  - Models have differing density requirements. To avoid polluting sensitivity analysis results, each model must be grid converged.
- Drive grid refinement to an insignificant component of overall modeling error.
  - Grid refinement error is one that can be readily reduced.
- Ensure refined grid regions needed for flow physics capture fully encompass the feature.
  - For example, wake refinement region must be large enough to prevent prediction of premature wake closure which will affect vehicle drag.

## “Respect the physics”

- Avoid attempting to drive unsteady problems to steady-state for example.
- Solvers typically do not converge and aero is inaccurate.

## Watch out for (code specific?) numerical issues

- i.e. strain based turbulence production can generate  $\mu_t$  at shocks and effect boundary layer and shoulder flow/wake behavior.

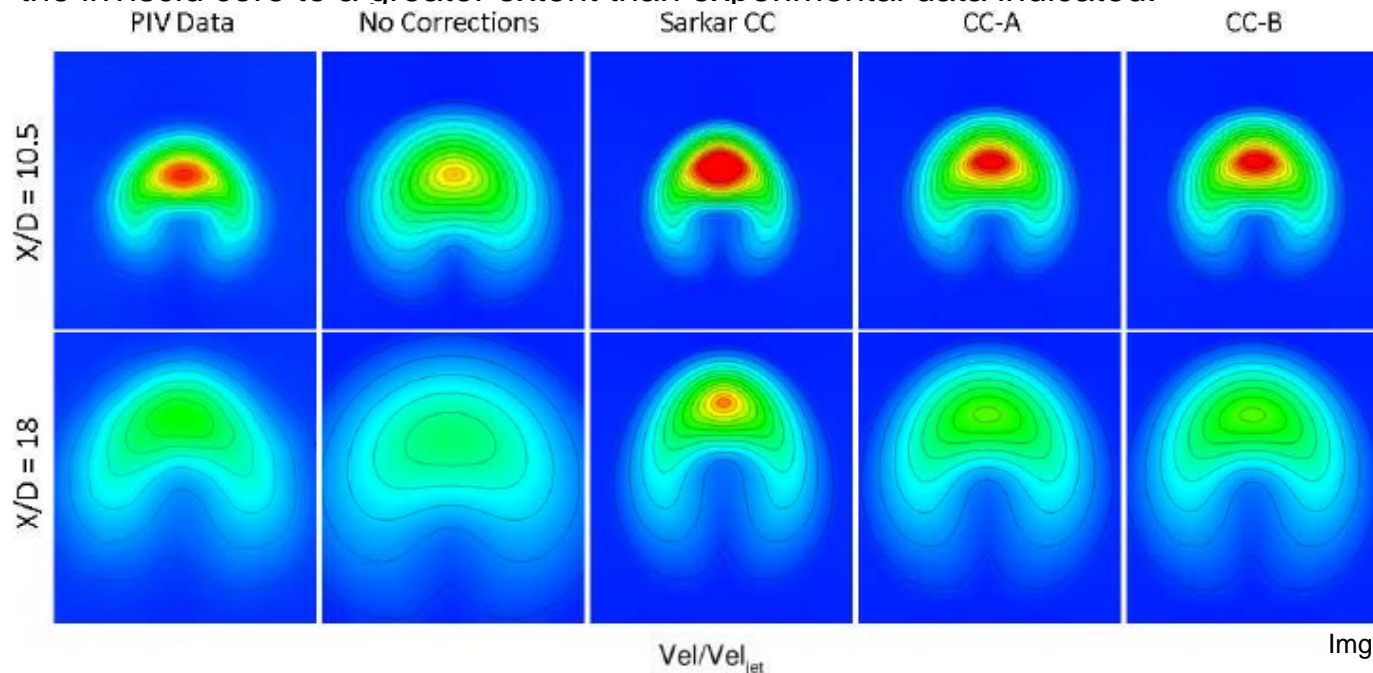


Img : Darby Vicker

# LAV/Plume issues

Orion is perhaps uniquely sensitive to plume modeling, but some lessons are general.

- Turbulence modeling has been the largest driver in CFD error for plume simulations.
  - Compressibility correction was widely regarded as necessary for our high exit Mach plumes, yet correlation with WTT data did not improve it's use.
  - Corrections tuned to an axial jets did not perform well for our inclined jet.
    - Performance varied with alpha/Mach, but standard Sarkar corrections tended to preserve the inviscid core to a greater extent than experimental data indicated.



Img : Nico Gross

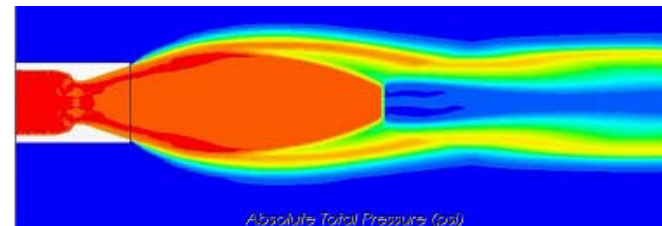
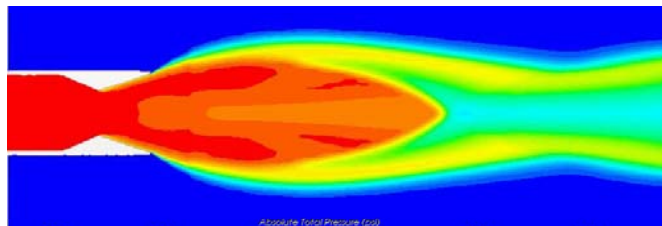


## LAV/Plume issues (cont)

**Survey of available turbulence models showed best match to experiment using SST.**

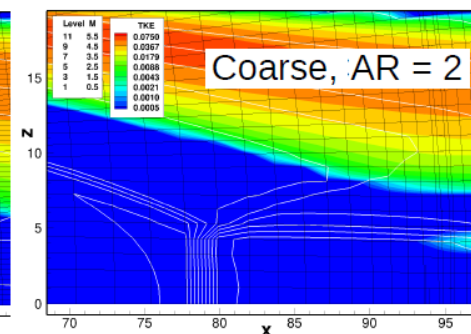
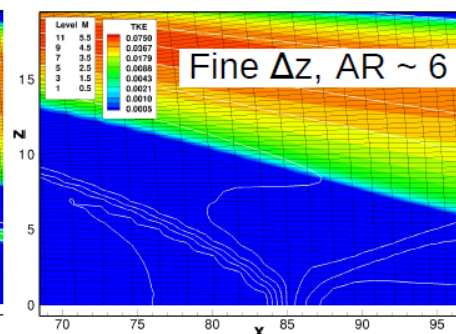
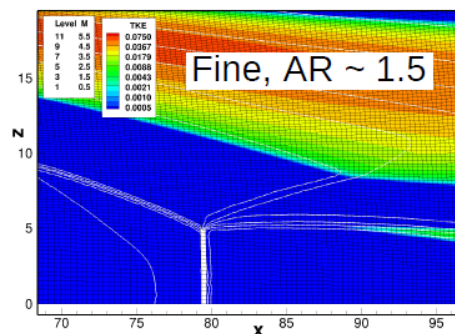
**Some conditions match well, others show poor experimental match**

- In some of these cases – Schlieren imagery from testing shows a mach disk where the CFD did not which drives plume shape.
  - Small changes in plenum geometry affect Mach disk formation



Img : John Melton/  
Robert Childs

- Mach disk prediction is also influenced by several numerical aspects.
  - Flux scheme, dissipation.
  - Cell aspect ratio

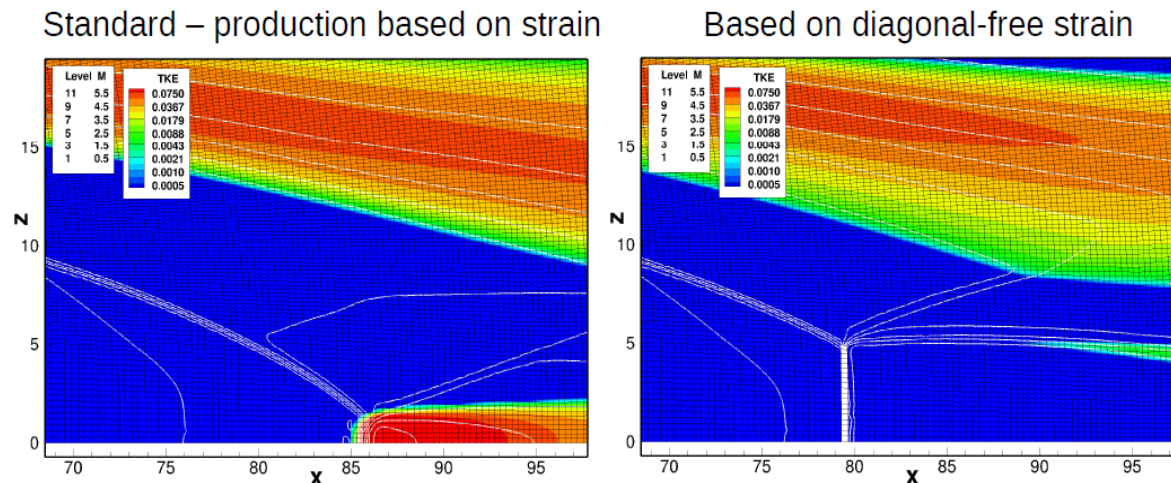


Img : Robert Childs



# LAV Plume analysis

- Mach disk (cont)
  - Generally expect this to be an inviscid flow feature, however, sensitivity to turbulence modeling has been seen.
    - SST turbulence kinetic energy production based on strain produced large TKE values through strong shocks.

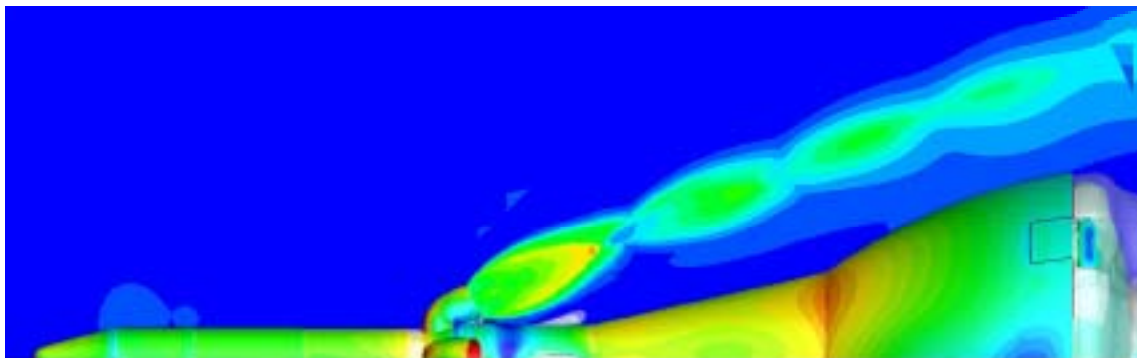


Img : Robert Childs

- Tends to pull shock disk downstream and/or lead to prediction of no Mach disk.
  - Using high dissipation for solution startup may lock soln into a prediction of no Mach disk
- Plume edge mixing/turbulence seen in full scale tests is not replicated in CFD
  - CFD plume spreading rate is lower in some cases
  - still investigating...

# Plume shear layer detail

CFD

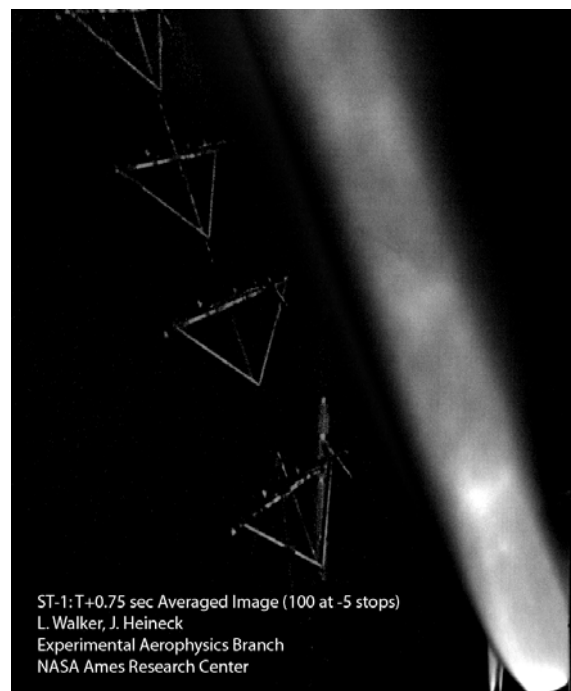


ST-1  
Experiment

50  $\mu$ s exposure



100 frame average = 5ms exposure



CFD and ST-1 not at same conditions

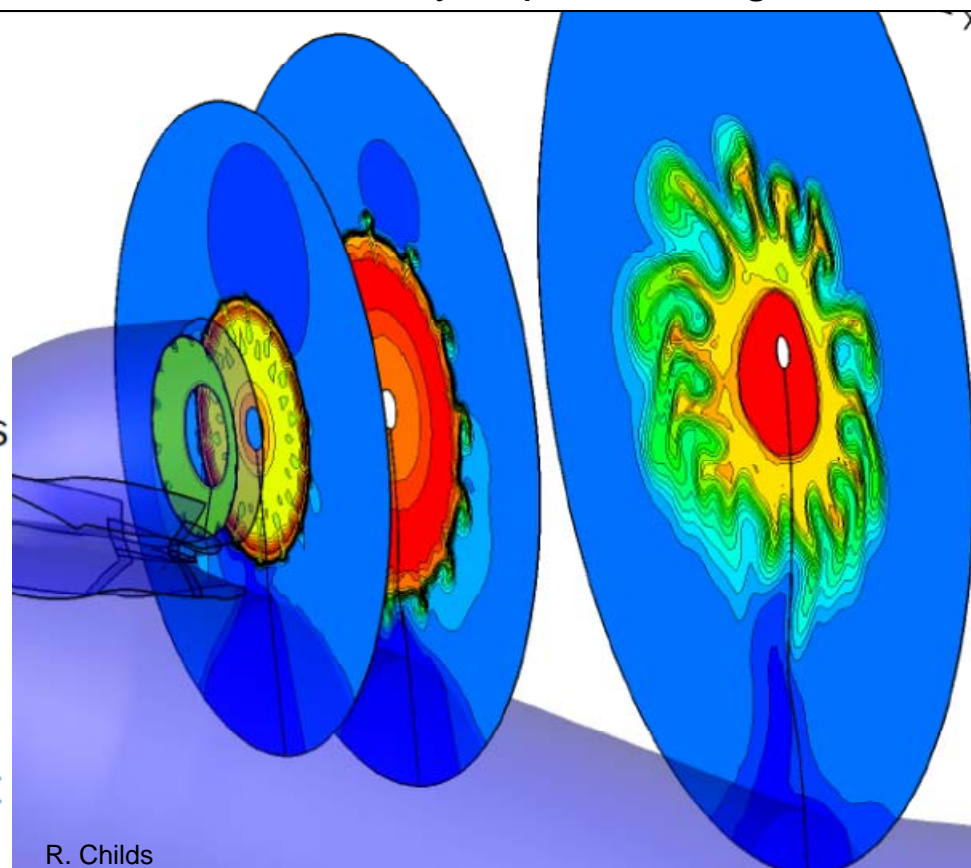
# Shear layer modeling

## Orion is sensitive to plume spreading rate and shear layer prediction

- OML/plume configuration places the plume boundary very near to the vehicle at the aft edge, causing large changes as plumes shift with flow conditions, thrust levels, or plume modeling differences.
- Path to fully modeling all aspects of this is not clear – likely expensive regardless...

- Investigated high resolution grid with vorticity seeding

- Streamwise vortices spawn low-speed streaks akin to boundary layer streaks
- Streaks trigger external Görtler vortices
- Physics of turbulence amplification seen, but far downstream



R. Childs



# Final Thoughts

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**From an aerodynamicist's perspective, the issues we have faced and are still facing are interesting problems to work on.**

- However, few of us are paid to conduct science experiments/basic physics research.

**Our goal is to provide the highest quality environments possible within the available resources.**

- Database accuracy needs depend on the system's robustness.

**Need for aerodynamics typically leads ability to produce it**

- Configuration still in flux, etc.
- Use lower fidelity tools for preliminary data with care/caution
  - Accuracy of tools can be highly configuration dependent and require skill/experience to obtain good results

**Good CFD results require a skilled operator**

- Fluids/aero experience with knowledge of the numerical models is ideal.

**Large compute power does not eliminate the need for quality control of each solution**

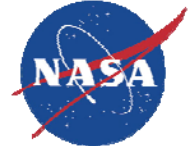
**Use of multiple sources of data to cross-validate is important**

- multiple codes, with high quality WTT data preferred
- Need increases for analysis outside of the core experience.

**Avoid designs that cannot be analyzed**

- Includes designs possible to characterize, but not within budget constraints.

# References



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## Turbulence Model Assessment for Hot Plumes (Invited)

Andrea Shestopalov Science and Technology Corporation, Mountain View, CA, UNITED STATES; Robert Childs Science and Technology Corporation, Mountain View, CA, UNITED STATES; John Melton NASA Ames Research Center, Moffett Field, CA, UNITED STATES

AIAA-2011-3340

29th AIAA Applied Aerodynamics Conference, Honolulu, Hawaii, June 27-30, 2011

## Overflow Simulation Guidelines for Orion Launch Abort Vehicle Aerodynamic Analyses (Invited)

Robert Childs Science and Technology Corporation, Hampton, VA; Joseph Garcia NASA Ames Research Center, Moffett Field, CA; John Melton NASA Ames Research Center, Moffett Field, CA; Stuart Rogers NASA Ames Research Center, Moffett Field, CA; Andrea Shestopalov Science and Technology Corporation, Hampton, VA; Darby Vicker NASA Johnson Space Center, Houston, TX

AIAA-2011-3163

29th AIAA Applied Aerodynamics Conference, Honolulu, Hawaii, June 27-30, 2011