Two-Dimensional Aeroelastic Flutter-Onset and Limit Cycle Oscillation Computations for the NASA Benchmark Supercritical Wing Configuration

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# Objectives and Approach

- Objective #1: Can a two-dimensional computational model predict results in the vicinity of the three-dimensional experimental results for the NASA Benchmark Super-critical Wing (BSCW) configuration?
- Objective #2: What sort of predicted aeroelastic Limit Cycle Oscillation (LCO) trends will the two-dimensional computational model yield? i.e., sub-critical or super-critical LCO response?
- Objective #3: Does the two-dimensional computational model predict transonic flow buffet?

Approach: A nonlinear frequency domain Harmonic Balance (HB) based Computational Fluid Dynamic (CFD) and aeroelastic solver, which allows for the direct computation of aeroelastic LCO response curves.

### Airfoil Aeroelastic Configuration Governing Equations



$$\begin{split} R_{1} &= \bar{\alpha}_{0} - \alpha_{e_{0}} - \frac{2V^{2}}{\pi r_{\alpha}^{2}} \bar{c}_{m_{0}} \\ R_{2} &= \left\{ \frac{\operatorname{Re}(\bar{c}_{I_{1}})}{\pi \tilde{\alpha}_{1}} - \frac{1}{4} \mu \tilde{\omega}^{2} \left[ \frac{m_{h}}{m} \operatorname{Re}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) + x_{\alpha} \right] \right\} V^{2} \\ &- \sqrt{\mu} \bar{\omega} \zeta_{h} \left( \frac{\omega_{h}}{\omega_{\alpha}} \right) \operatorname{Im}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) V + \left( \frac{\omega_{h}}{\omega_{\alpha}} \right)^{2} \operatorname{Re}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) \\ R_{3} &= - \left\{ 2 \frac{\operatorname{Re}(\bar{c}_{m_{1}})}{\pi \bar{\alpha}_{1}} + \frac{1}{4} \mu \tilde{\omega}^{2} \left[ x_{\alpha} \operatorname{Re}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) + r_{\alpha}^{2} \right] \right\} V^{2} \\ &+ r_{\alpha}^{2} \\ R_{4} &= \left[ \frac{\operatorname{Im}(\bar{c}_{I_{1}})}{\pi \bar{\alpha}_{1}} - \frac{1}{4} \mu \tilde{\omega}^{2} \frac{m_{h}}{m} \operatorname{Im}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) \right] V^{2} \\ &- \sqrt{\mu} \bar{\omega} \zeta_{h} \left( \frac{\omega_{h}}{\omega_{\alpha}} \right) \operatorname{Re}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) V + \left( \frac{\omega_{h}}{\omega_{\alpha}} \right)^{2} \operatorname{Im}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) \\ R_{5} &= - \left[ 2 \frac{\operatorname{Im}(\bar{c}_{m_{1}})}{\pi \bar{\alpha}_{1}} + \frac{1}{4} \mu \tilde{\omega}^{2} x_{\alpha} \operatorname{Im}\left( \frac{\bar{h}_{1}}{\bar{\alpha}_{1} b} \right) \right] V^{2} \\ &+ \sqrt{\mu} \bar{\omega} V \zeta_{\alpha} r_{\alpha}^{2} \end{split}$$

NASA BSCW Aeroelastic Configuration Transonic RANS CFD Model

Structural Parameters:  $x_{\alpha} = 0.0, r_{\alpha}^{2} = 1.024, (\omega_{h}/\omega_{\alpha}) = 0.646,$   $\zeta_{h} = 0.002, \zeta_{\alpha} = 0.002,$  $a = 0.0, \text{ and } \alpha_{e_{0}} = 5.0^{\circ}.$ 

Computational Grid - 193  $\times$  49 "O-Mesh":



Figure: Computational Grid.

### NASA BSCW Aeroelastic Configuration Transonic RANS CFD Model Continued

Flow Near the Flutter-Onset Condition:  $M_{\infty} = 0.80, Re_{\infty} \approx 4,000,000, \bar{\alpha}_0 \approx 6.15^{\circ}$ , and  $\mu \approx 1100$ .



Figure: Mean Flow Mach Number Contours.

## Airfoil Geometric Shape Definition / Might "Better" Tabulated Data Be Available? Tabulated data is only given to at most three significant figures.

Table XIX. Coordinates of 14-Percent-Thick Supercritical Airfoil SC(2)-0414 Designed for 0.4 Lift Coefficient

|       |        |        | -   |       |       |        |
|-------|--------|--------|-----|-------|-------|--------|
| x/c   | (y/c)  | (y/c). |     | x/c   | (y/c) | (v/o). |
|       | 00     | a1     |     |       | 11    | 131-11 |
| 0.000 | 0.0000 | 0.0000 |     | .500  | .0684 | 0642   |
| .002  | .0108  | 0108   |     | .510  | .0680 | 0633   |
| .010  | 0225   | = 0225 |     | 530   | 0672  | - 0612 |
| .020  | .0299  | -,0299 |     | .540  | .0667 | 0600   |
| .030  | .0350  | 0350   |     | .550  | .0662 | 0587   |
| .040  | .0389  | 0389   |     | .560  | .0656 | 0573   |
| .050  | .0421  | 0421   |     | .570  | .0650 | 0558   |
| .060  | .0448  | 0448   |     | .580  | .0643 | 0543   |
| .070  | 0491   | - 0493 |     | .590  | 0636  | =.0527 |
| .090  | .0510  | 0512   |     | -610  | .0620 | 0492   |
| .100  | .0527  | 0529   |     | .620  | .0611 | 0474   |
| .110  | .0542  | 0545   |     | .630  | .0602 | -,0455 |
| .120  | .0556  | 0560   |     | .640  | .0593 | 0435   |
| .130  | ,0569  | 0573   |     | .650  | .0583 | 0415   |
| .140  | .0581  | 0585   |     | .660  | .0573 | 0394   |
| -150  | .0592  | 0597   |     | .670  | .0562 | 0373   |
| 170   | 0612   | = 0618 |     | 690   | 0540  | - 0332 |
| .180  | .0621  | 0627   |     | .700  | .0528 | 0308   |
| .190  | .0629  | 0636   |     | .710  | .0516 | 0286   |
| .200  | .0637  | 0644   |     | .720  | .0503 | 0264   |
| .210  | .0644  | 0651   |     | .730  | .0490 | 0242   |
| .220  | .0651  | 0658   |     | .740  | .0477 | 0220   |
| .230  | .0657  | 0664   |     | .750  | 0464  | 0198   |
| .250  | 0668   | 0675   |     | .770  | .0436 | 0156   |
| .260  | .0673  | 0680   |     | .780  | .0422 | 0136   |
| .270  | .0677  | 0684   |     | .790  | .0407 | 0116   |
| .280  | 0681   | 0688   |     | .800  | .0392 | 0097   |
| .290  | .0685  | 0691   |     | .810  | .0377 | 0078   |
| .300  | .0688  | 0694   |     | .820  | .0362 | 0060   |
| .320  | .0693  | 0698   |     |       | .0346 | 0043   |
| .330  | .0695  | 0699   |     | .850  | .0314 | 0012   |
| .340  | .0697  | 0700   |     | .860  | .0298 | .0001  |
| .350  | .0699  | 0700   |     | .870  | .0281 | .0013  |
| .360  | .0700  | 0700   |     | .880  | .0264 | .0023  |
| .370  | .0701  | 0699   | - 1 | .890  | .0247 | .0032  |
| .190  | .0702  | 0698   |     | .910  | .0211 | .0044  |
| .400  | .0702  | 0695   |     | .920  | .0193 | .0046  |
| .410  | .0702  | 0693   | 1   | .930  | .0175 | .0046  |
| .420  | .0701  | 0690   | 1   | .940  | .0156 | .0043  |
| .430  | .0700  | 0686   | - 1 | .950  | .0137 | .0038  |
| .440  | .0699  | 0682   |     | .960  | .0117 | .0031  |
| .450  | .0697  | 0677   |     | .970  | .0097 | .0021  |
| 470   | .0693  | 0672   |     | . 780 | .0076 | - 0008 |
| .480  | .0690  | 0659   | -1  | 1.000 | .0033 | 0027   |
| .490  | .0687  | 0651   |     |       |       |        |
|       |        |        | - 6 |       |       |        |

### Figure: Airfoil Definition from Harris<sup>1</sup>

<sup>&</sup>lt;sup>1</sup>Charles D. Harris. NASA Supercritical Airfoils - A Matrix of Family Related Airfoils. NASA Technical Paper 2969. Mar. 1990.

#### NASA BSCW Aeroelastic Configuration Improved Airfoil Definition



Figure: Airfoil Surface Pressure.

Figure: Airfoil Surface Pressure - Close-up.



NASA BSCW Aeroelastic Configuration Computed LCO Unsteady Pitch Response Trend

NASA BSCW Aeroelastic Configuration Computed LCO Frequency Response Trend





NASA BSCW Configuration Computed LCO Aeroelastic Mode Shape Response Trend



