

AePW-3 – Third Aeroelastic Prediction Workshop

Coupled Numerical Simulation of Fluid-Structure Interaction

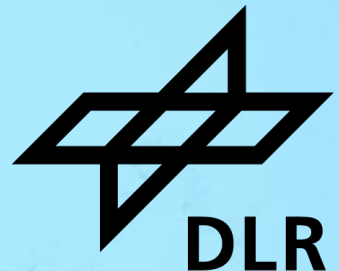
Bodo Reimann

German Aerospace Center (DLR)

Braunschweig, Germany

AePW-3 – Progress meeting

Online, 2024 June 27



Institute of Aerodynamics and Flow Technology

German Aerospace Center (DLR)



DLR – R&T Aeronautics, Space, Energy, Transport and Security
DLR – German Space Agency
DLR – Project Office

Institute	DLR total
3 sites	30 sites + 4 int. offices
~350 employees	~11.000 employees

Departments of the Institute

Experimental Methods
Ground Vehicles
Helicopters
High Speed Configurations
Spacecraft
Supersonic and Hypersonic Technologies
Technical Acoustics
Transport Aircraft
Wind Energy
Center for Computer Applications in AeroSpace Science and Engineering C²A²S²E

Spacecraft Department

Hypersonics
Aerothermodynamics
HEG Shock Tunnel
Rarefied Gas Dynamics
Satellite Thrusters (electric + chemical)
Numerics (DLR TAU-Code)

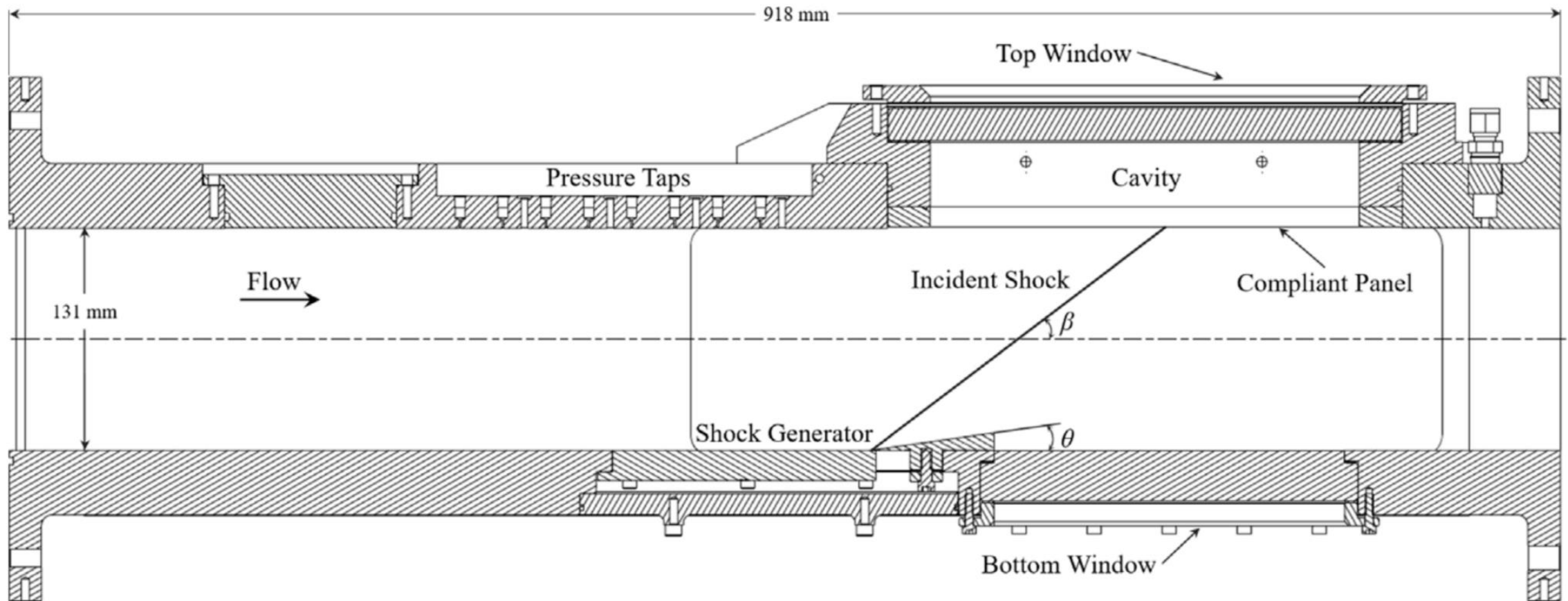
Köln

Braunschweig

Göttingen

Task

ARFL RC-19 Test Cell¹ Dayton, Ohio

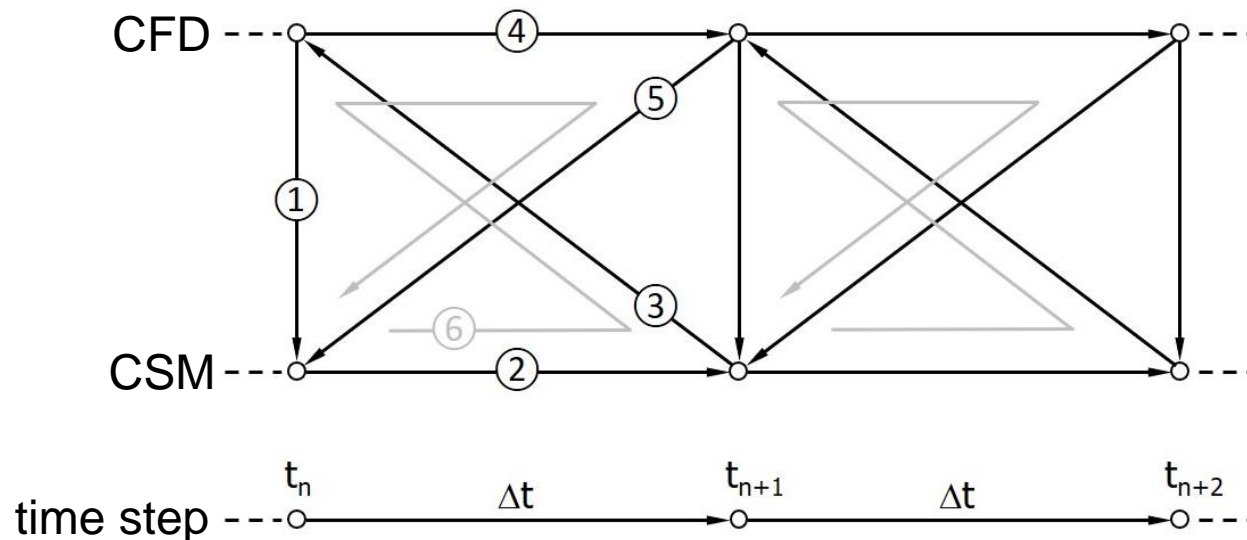


¹ K. B. Brouwer et al., J Fluids and Structures 108 (2022), <https://doi.org/10.1016/j.jfluidsstructs.2021.103429>

Coupling Scheme

CFD/CFM CFD/CSM

- CFD in-house solver DLR TAU-Code
- Flight dynamics solver, CFM (Reent 6D, 6-DoF TAU module solving Newton's second law and Euler equation)
- Structural mechanic solver, CSM (ANSYS, NASTRAN, B2000++pro)
- Partitioned approach with „strong coupling“



Coupled
Numerical
Fluid
Flight Mechanics
And
Structure
Simulations

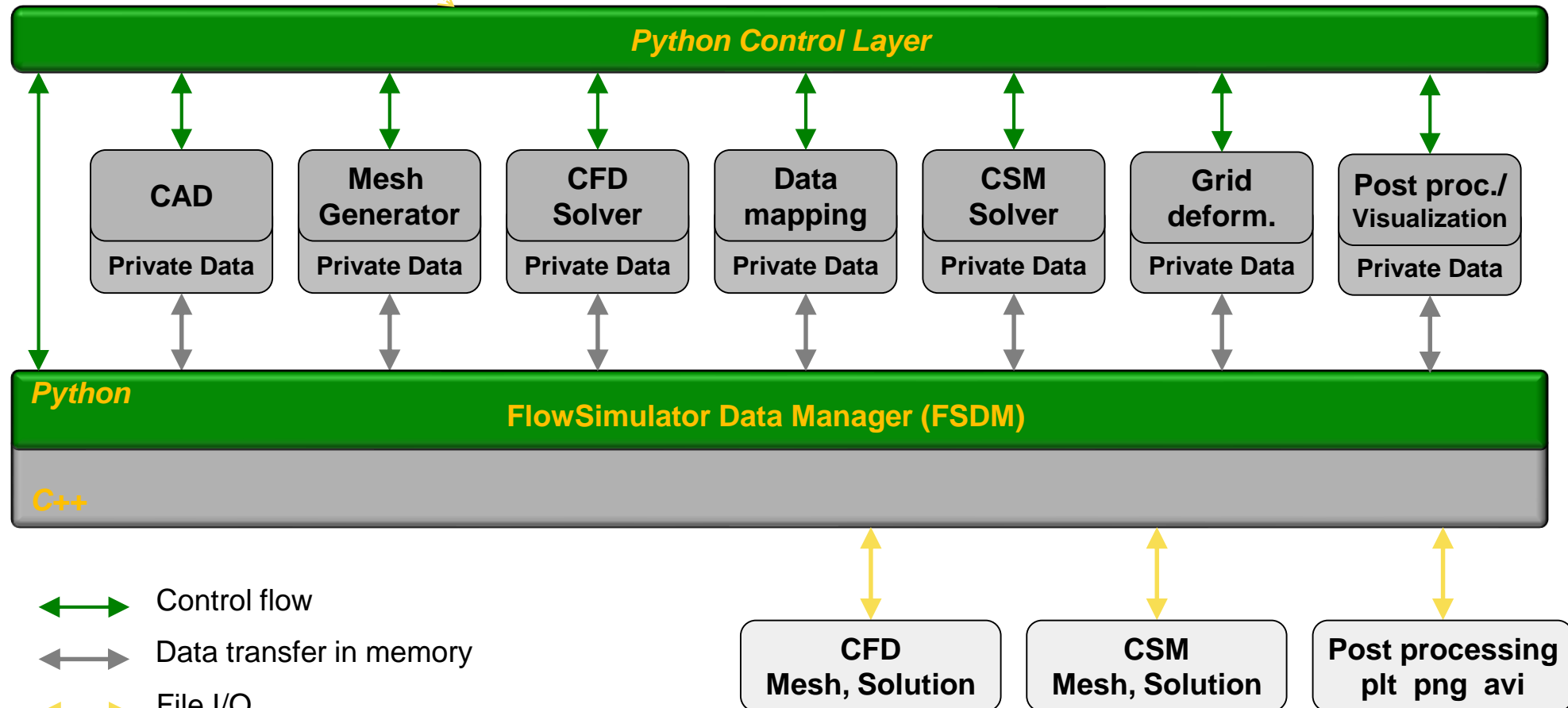
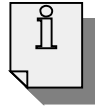


- ①, ③ and ⑤ exchange of coupling quantities
- ② computation of CSM time step
- ④ computation of CFD time step
- ⑥ repetition until convergence

FlowSimulator – Scheme FSI



FlowSimulator
script/parameters



Computational Domain

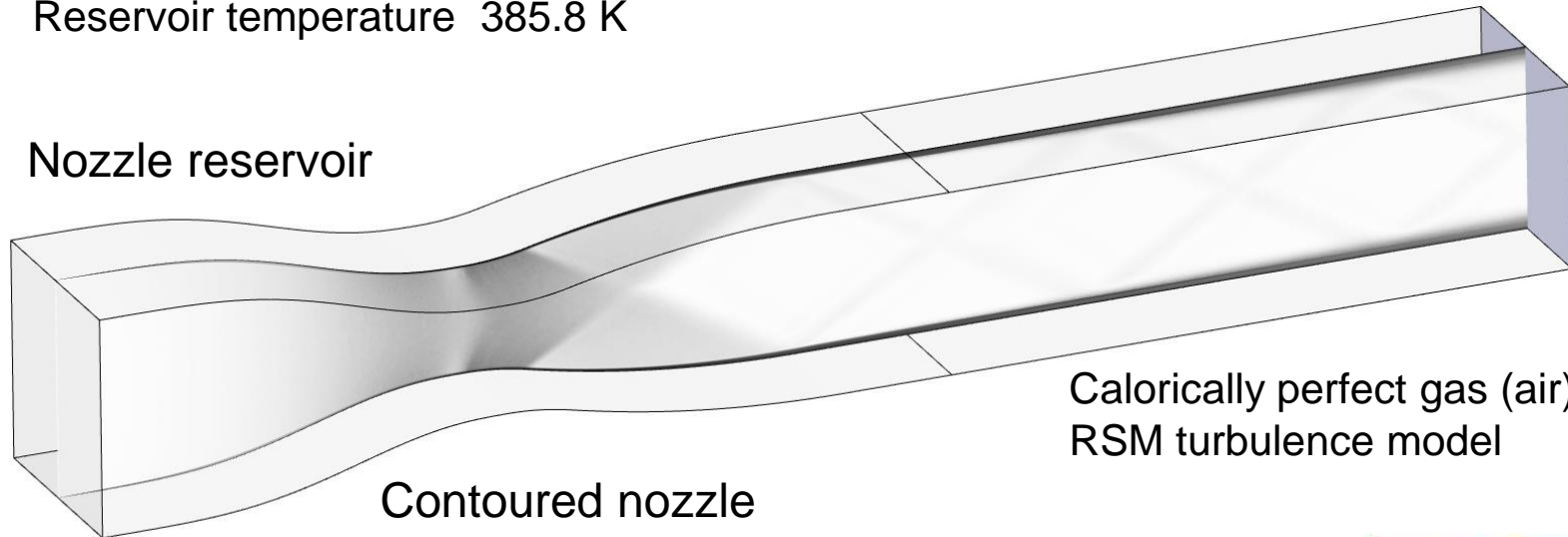
Steady-state Initial Condition



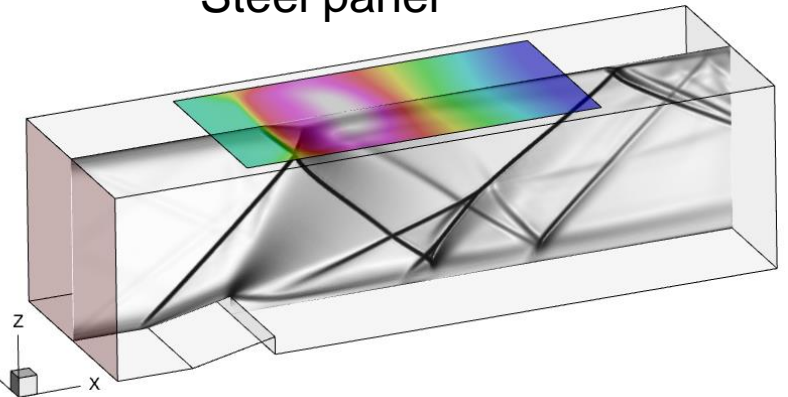
Reservoir pressure 344.85 kPa
Reservoir temperature 385.8 K

Dirichlet boundary

Nozzle reservoir



Contoured nozzle

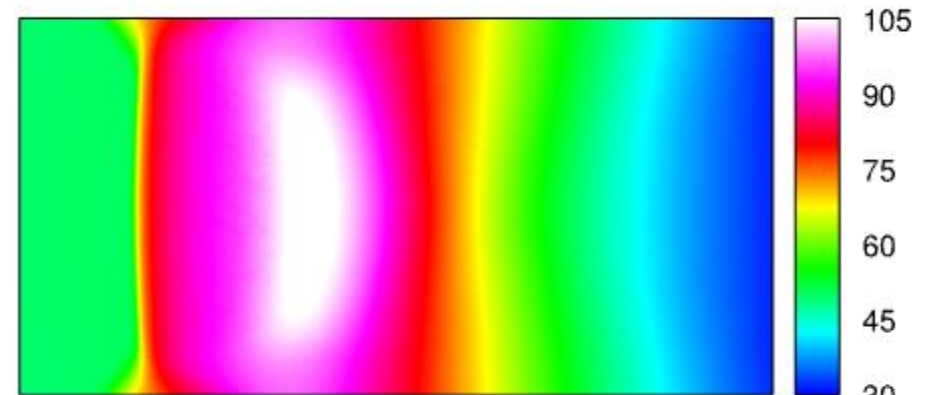


Steel panel

Shock generator (12° wedge)

Calorically perfect gas (air)
RSM turbulence model

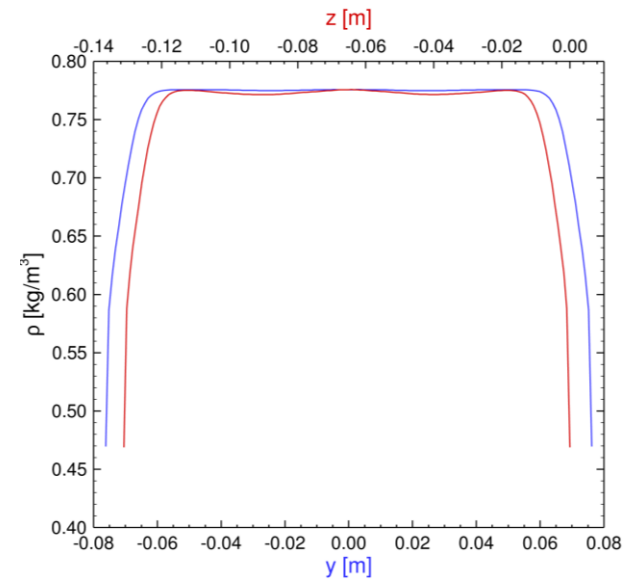
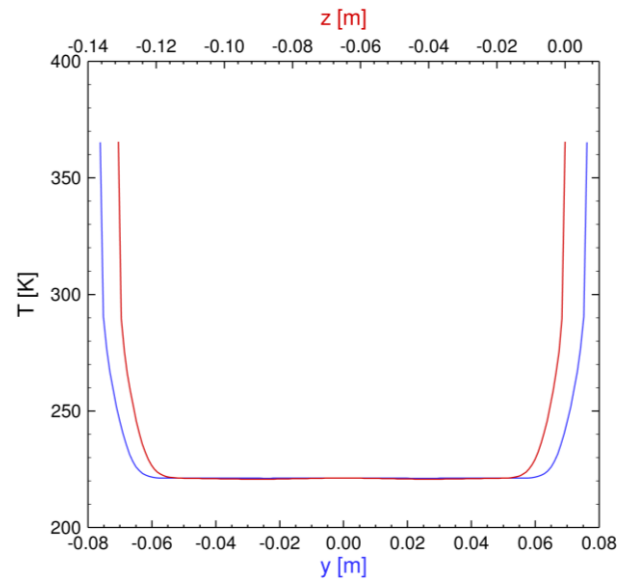
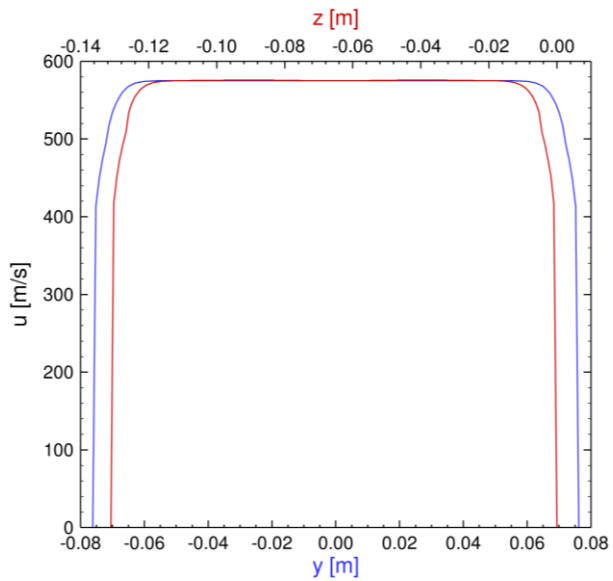
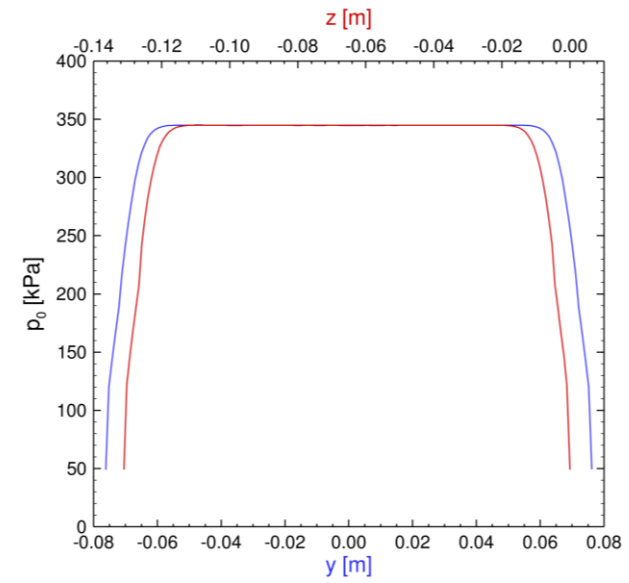
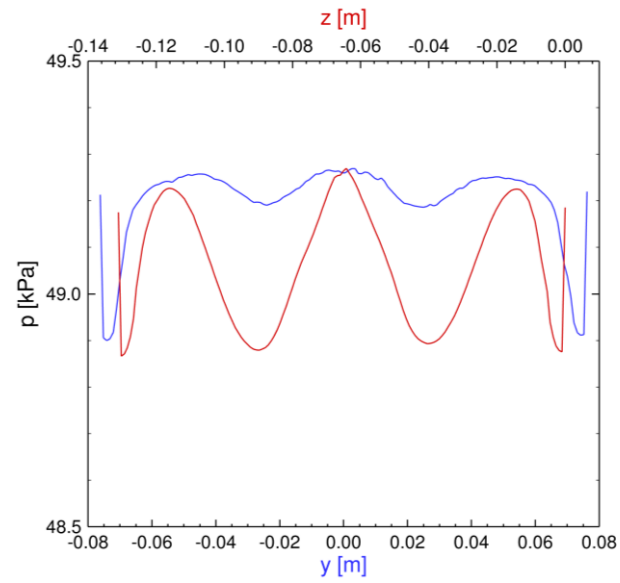
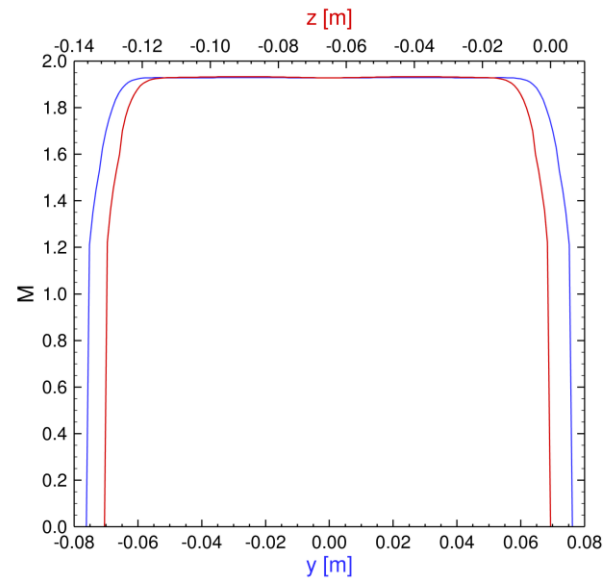
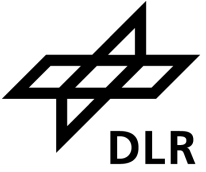
Panel size 253.9 x 127.0 x 0.635 mm
Material ASIS 4140 alloy
Density 7850 kg/m³
Poisson's ration 0.27
Young's modulus 2.08 Gpa
Thermal expansion coefficient 11.1 10⁻⁶ 1/K
Specific heat 460 J/(kg K)



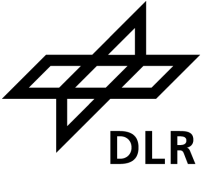
Surface pressure distribution

p [kPa]

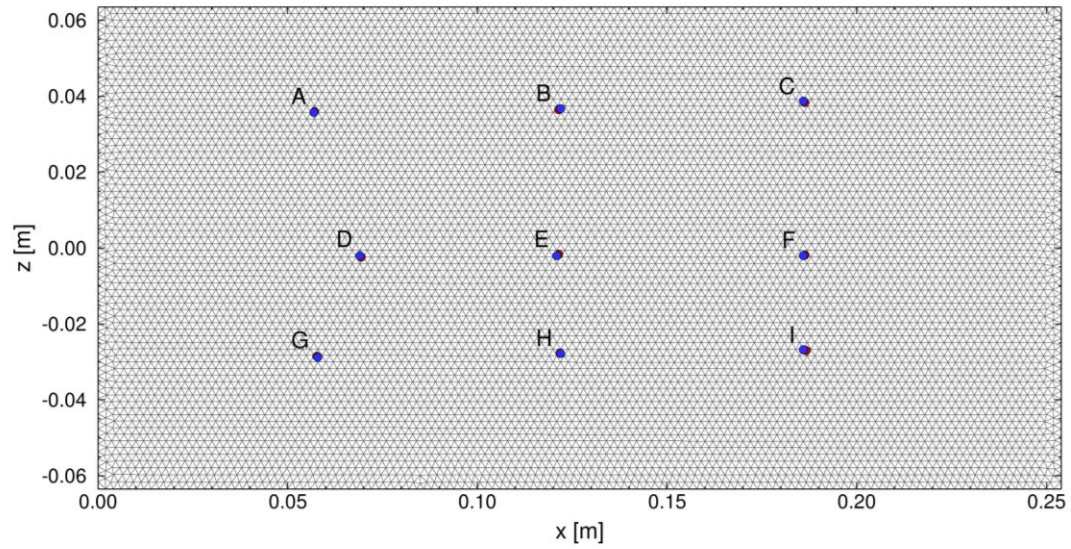
Inflow Profiles



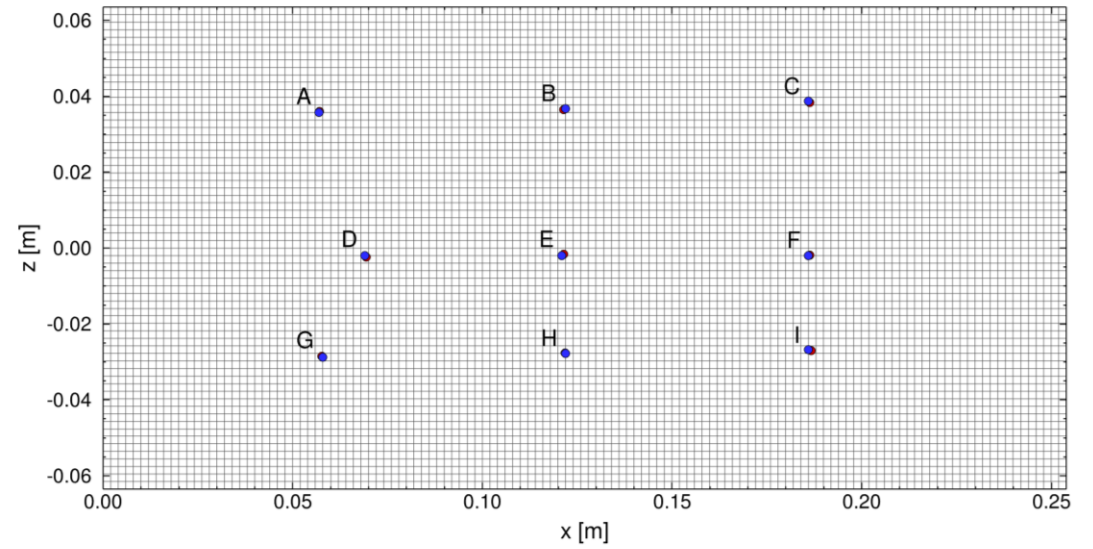
Panel Grid



CFD grid

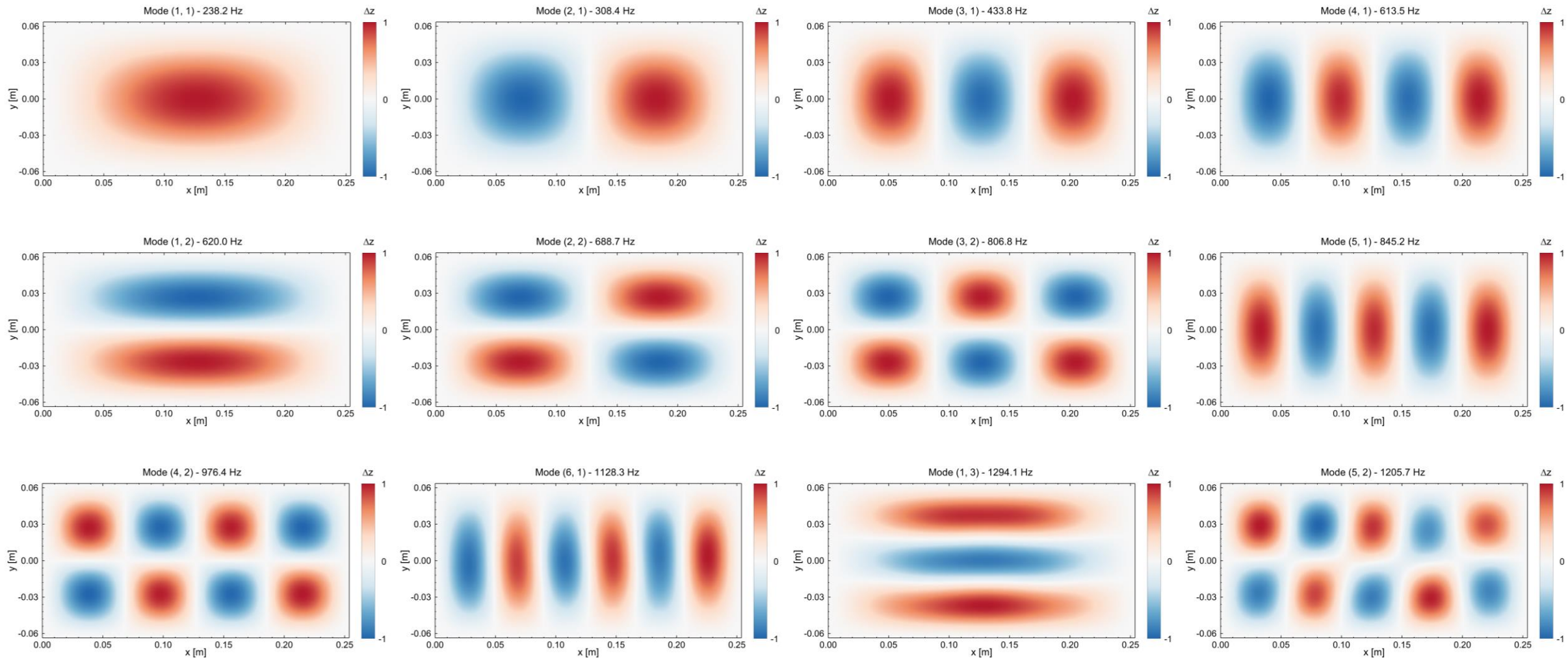
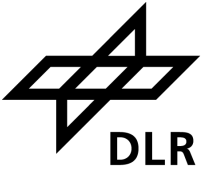


CSM grid

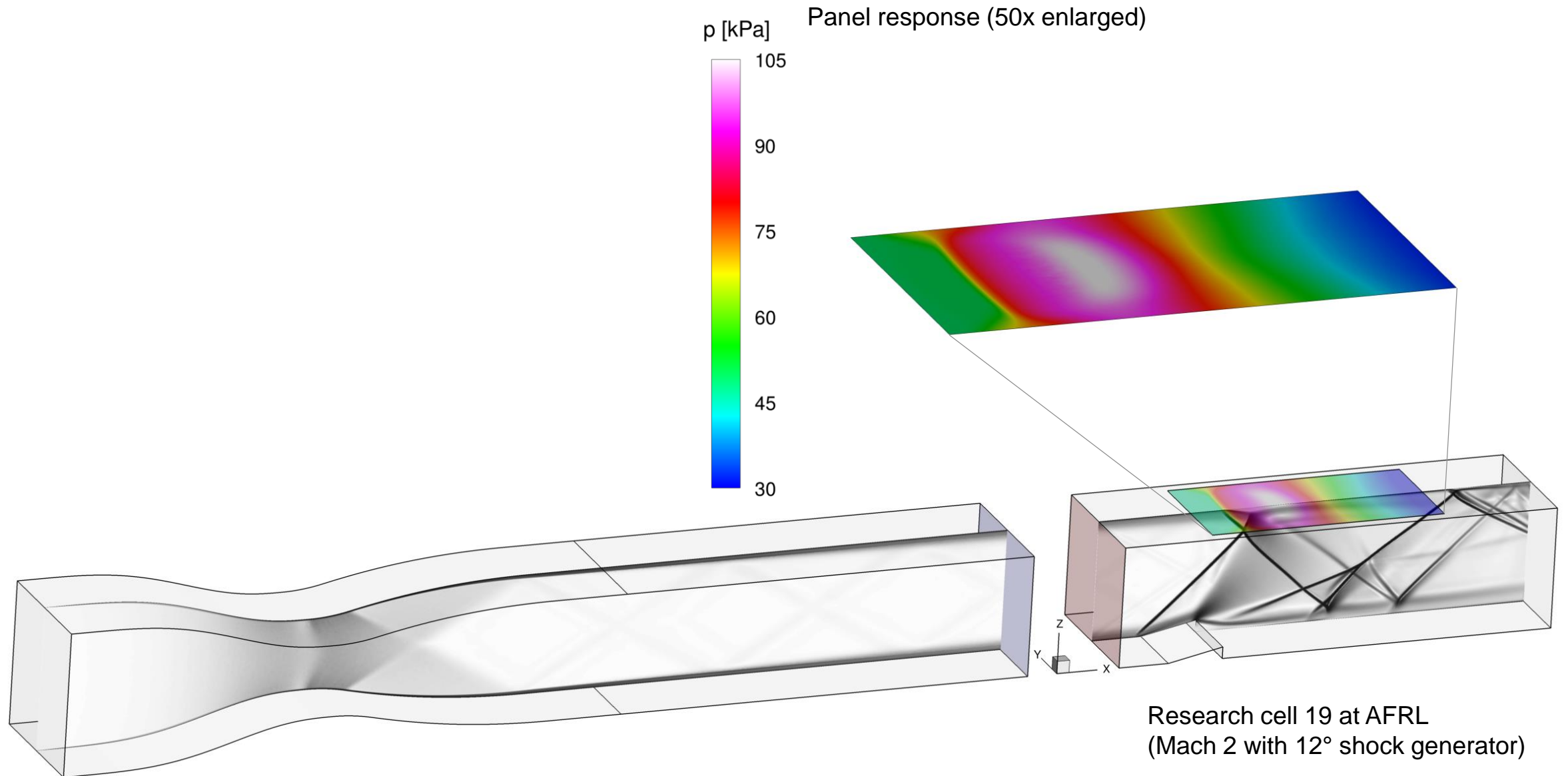


Modal Analysis

Natural Modal Frequencies ($\Delta T=0K$)



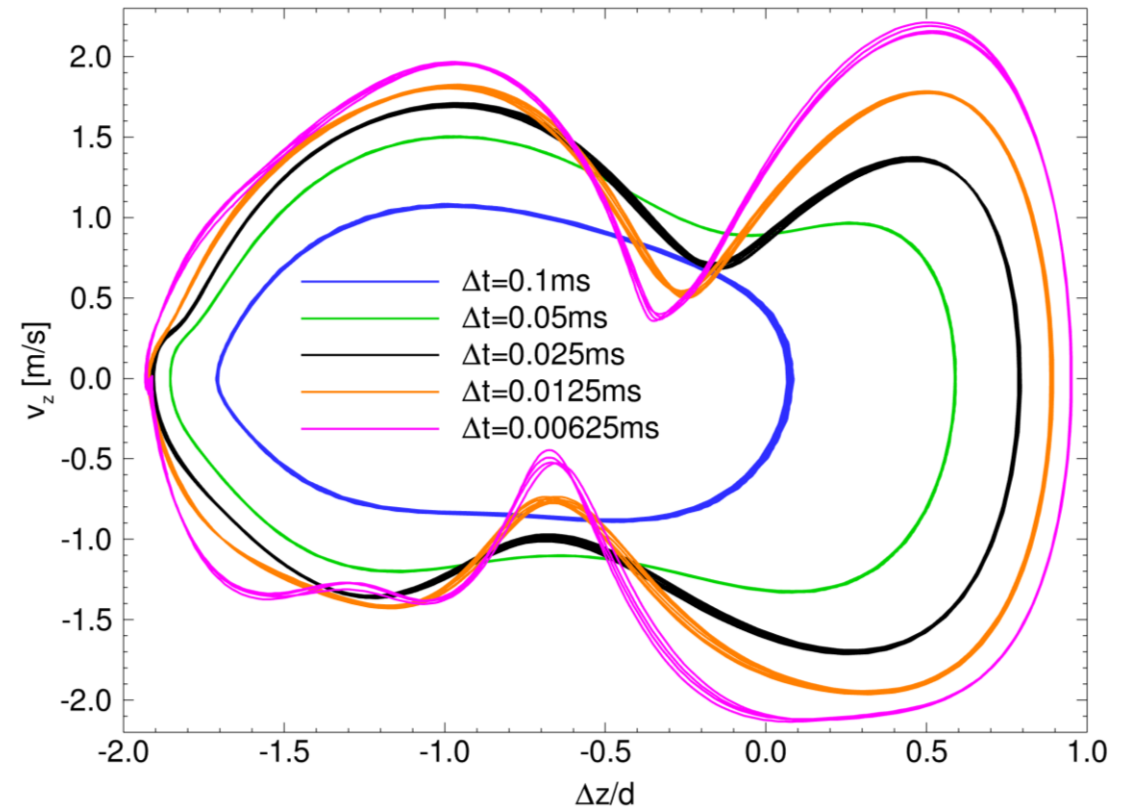
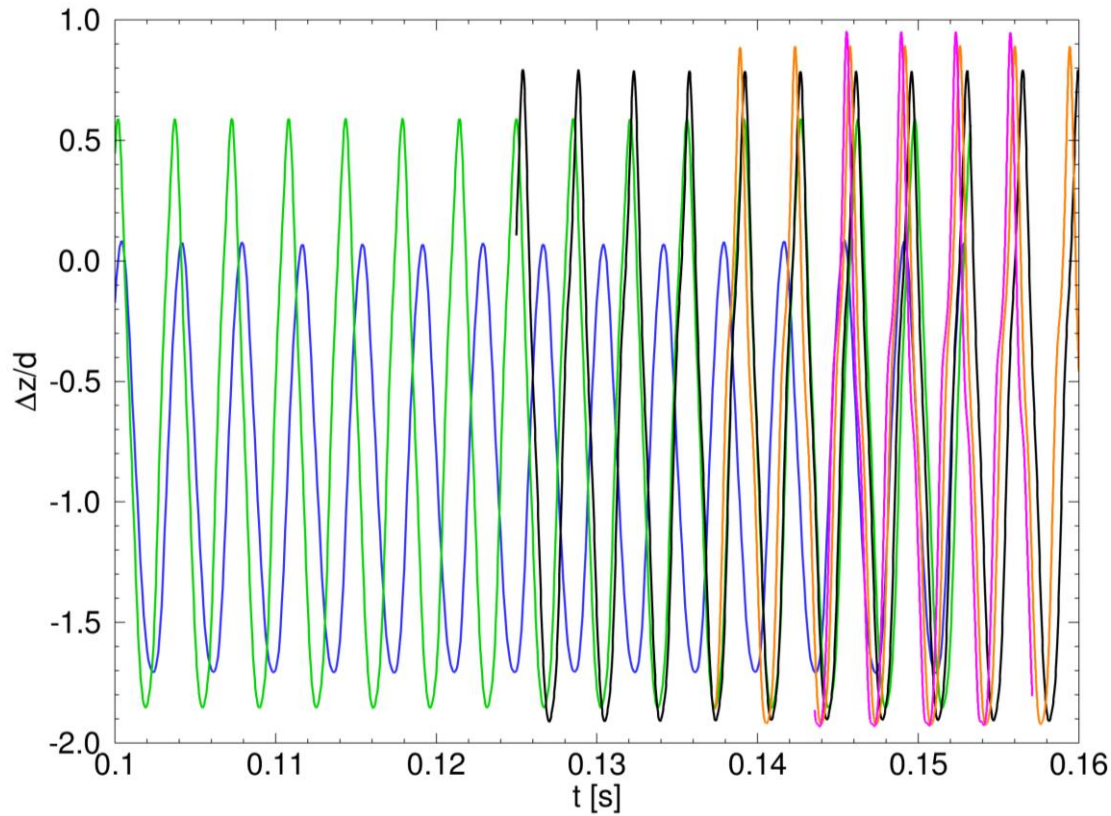
Flexible Panel Excited by Turbulent SBLI



Flow field Shadowgraph

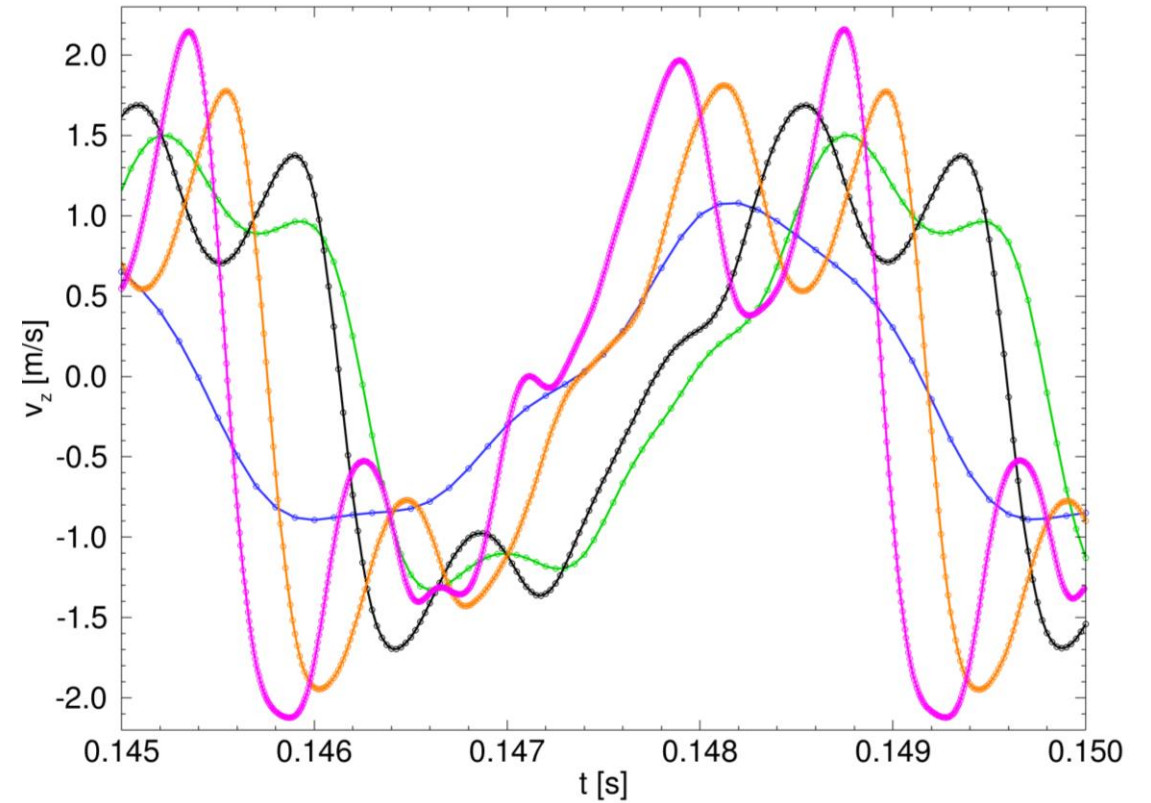
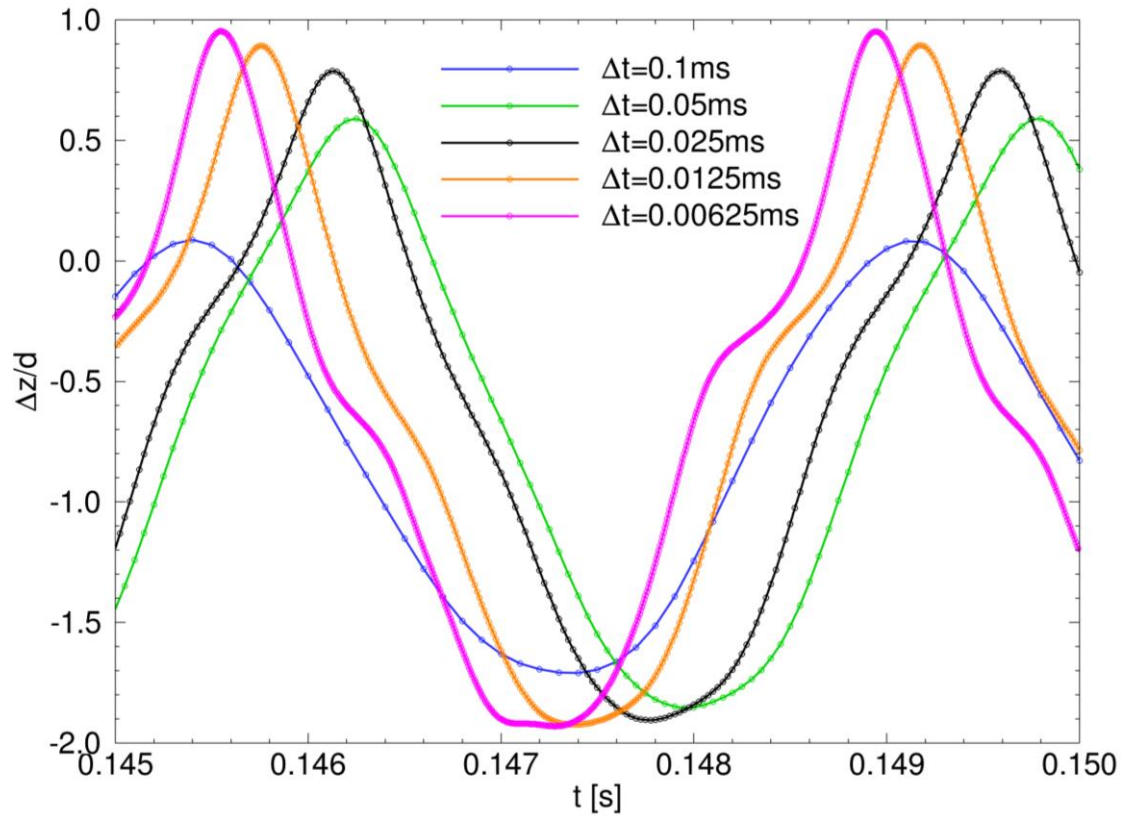
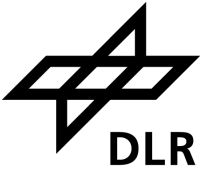


RC-19 Limit Cycle (12° Shock Generator, $\Delta T=12\text{K}$, $p_c = 92.355\text{kPa}$) @point E $x/L=0.5$ $y/L=0.25$



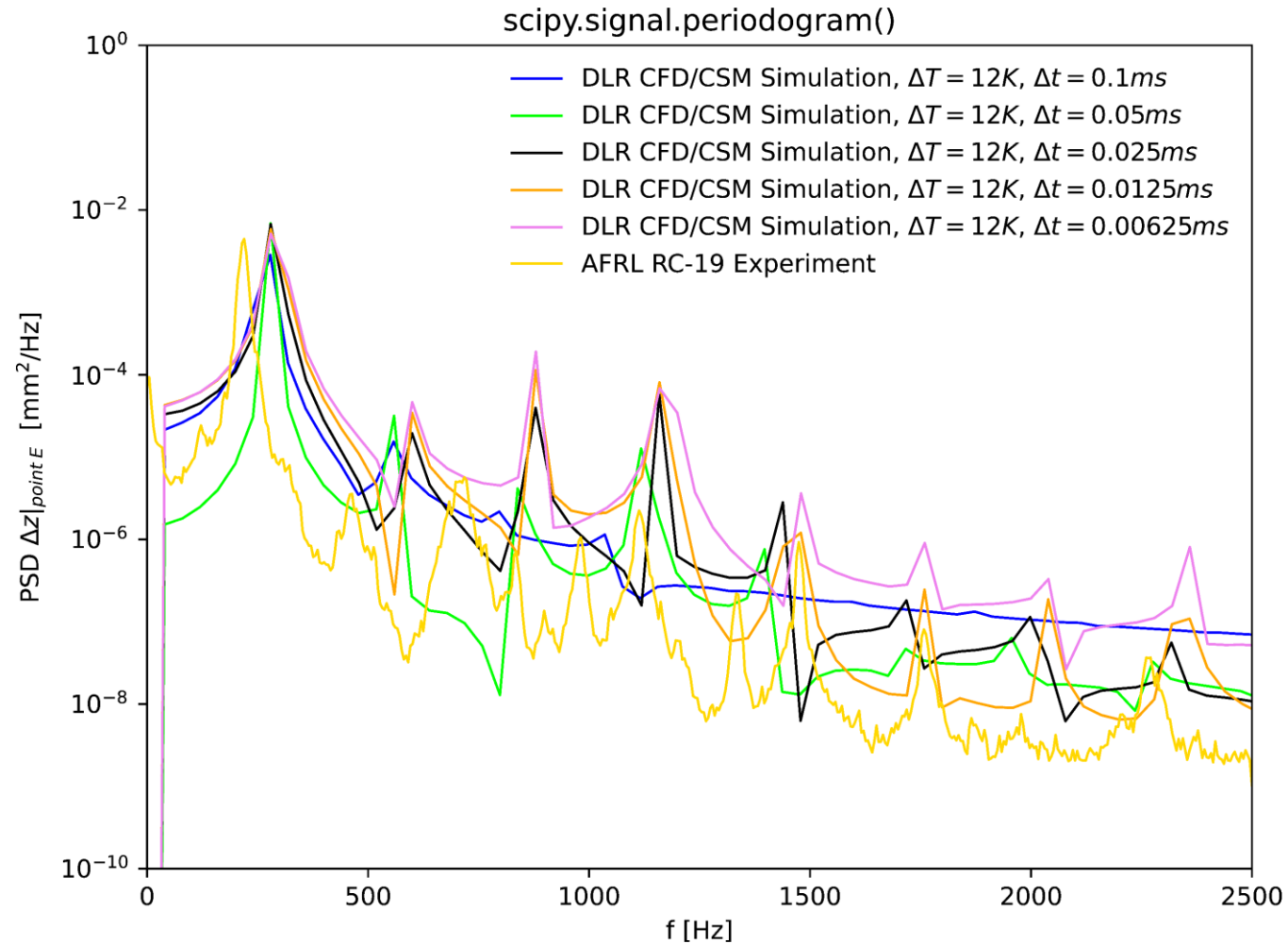
without structural damping and variable cavity pressure

RC-19 Limit Cycle (12° Shock Generator, $\Delta T=12\text{K}$, $p_c = 92.355\text{kPa}$) @point E $x/L=0.5$ $y/L=0.25$



without structural damping and variable cavity pressure

RC-19 Limit Cycle (12° Shock Generator, $\Delta T=12K$, $p_c = 92.355kPa$) @point E $x/L=0.5$ $y/L=0.25$



without structural damping and variable cavity pressure

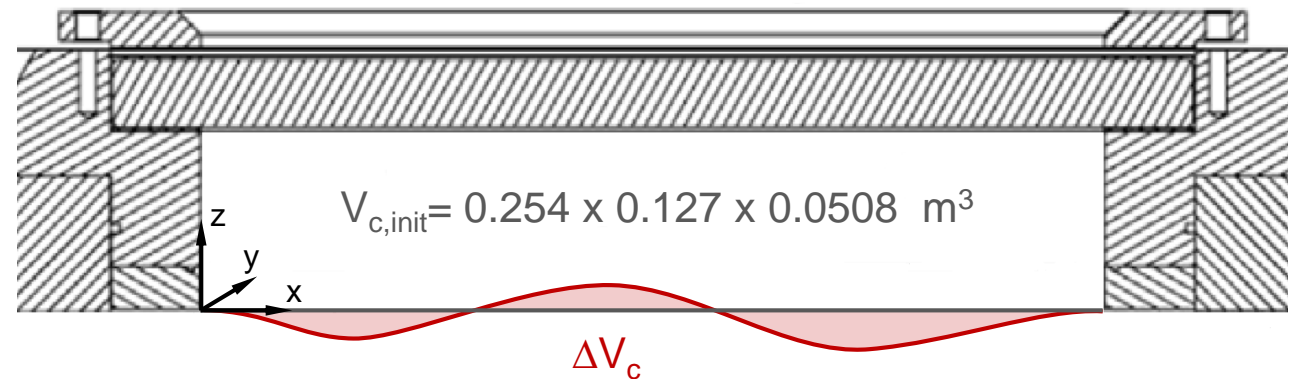
Rayleigh damping model

$$D_{ij} = \alpha_d M_{ij} + \beta_d K_{ij} \quad \alpha_d = 15, \quad \beta_d = 8 \cdot 10^{-7}$$

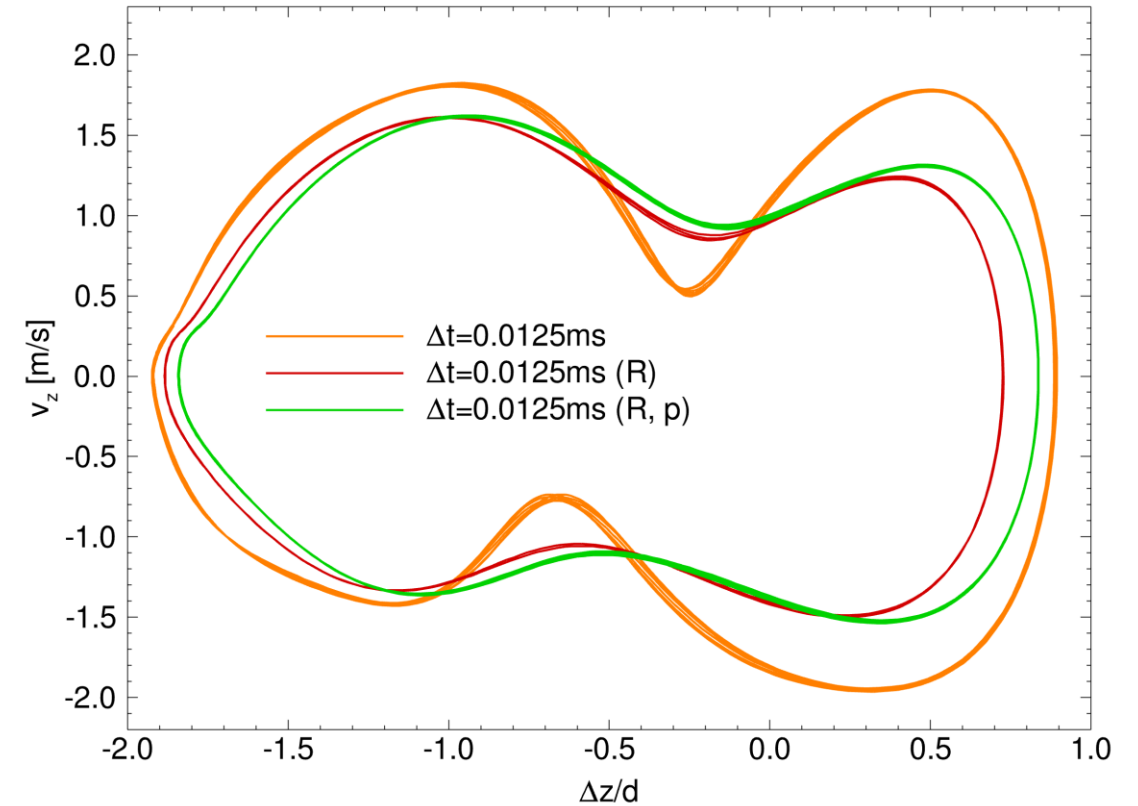
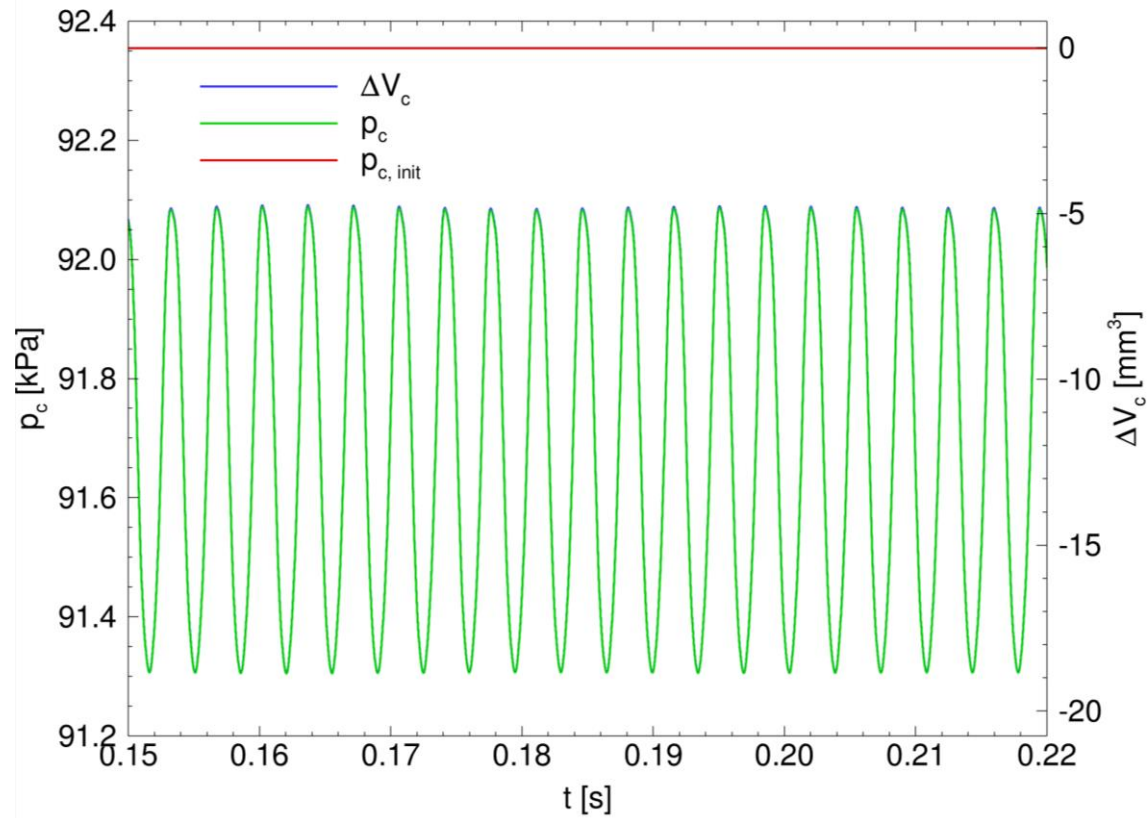
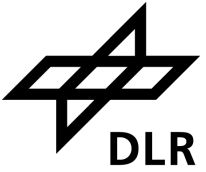
Cavity pressure model

$$\Delta V_c(t) = \iint_{\text{panel}} z(t, x, y) dx dy$$

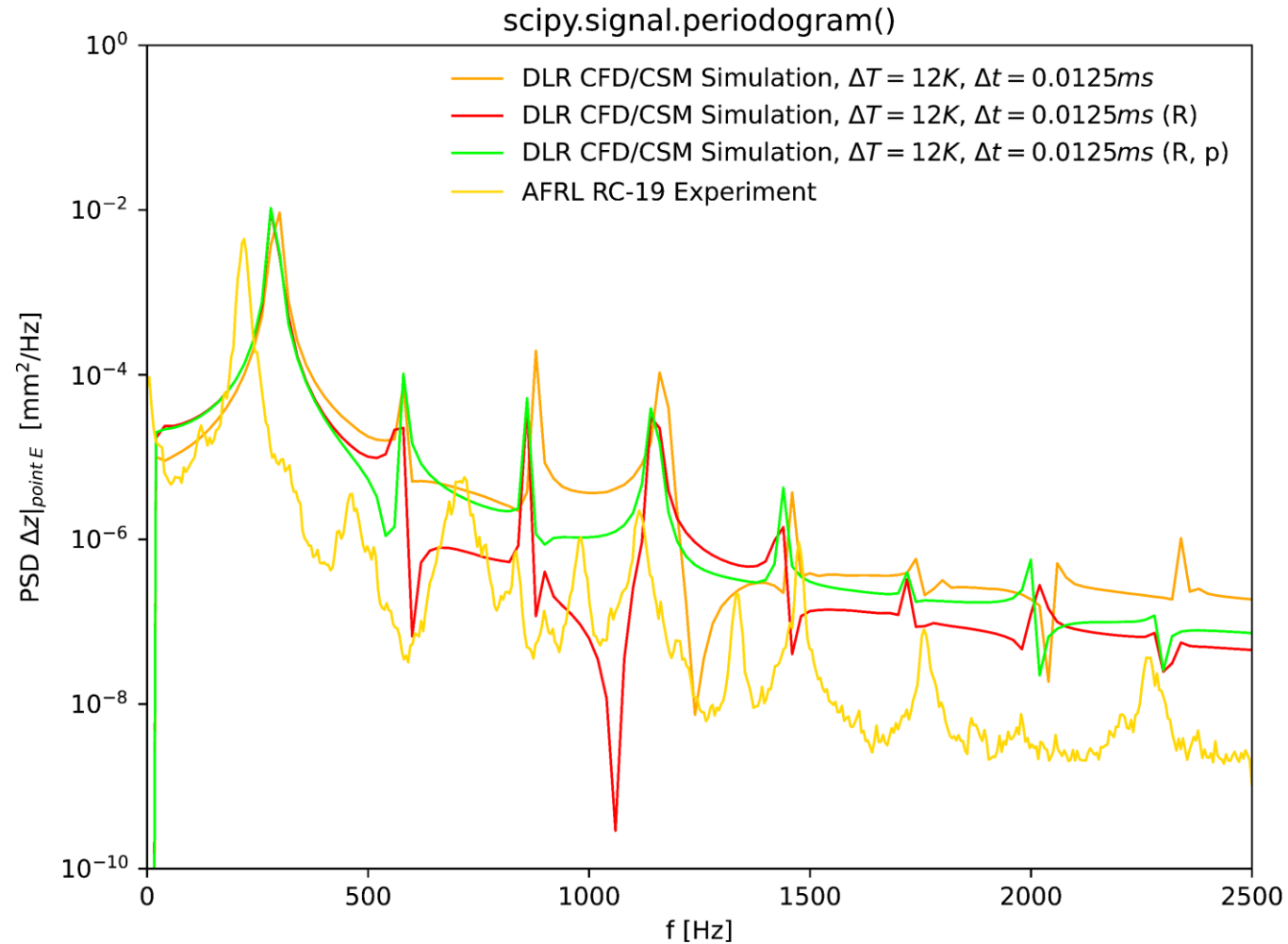
$$p_c(t) = \frac{p_{c,\text{init}} V_{c,\text{init}}}{V_{c,\text{init}} - \Delta V_c(t)}$$



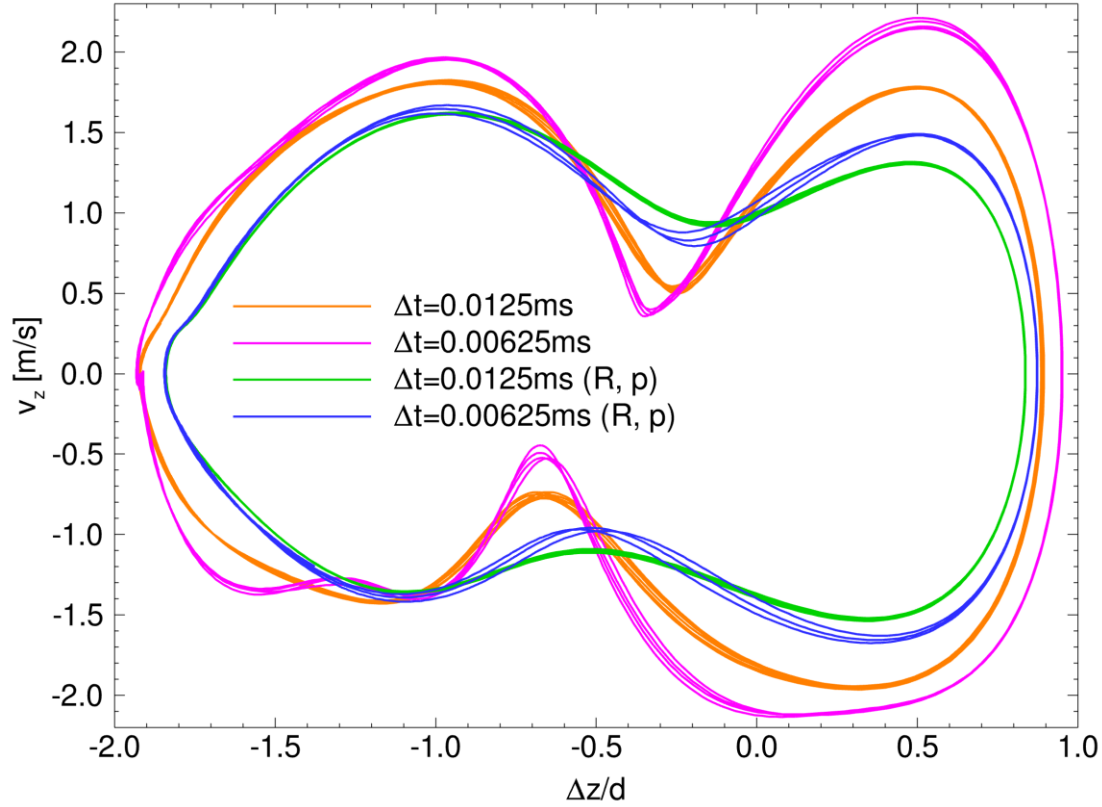
RC-19 limit cycle (12° Shock Generator, $\Delta T=12\text{K}$, $p_c = 92.355\text{kPa}$) @point E $x/L=0.5$ $y/L=0.25$



RC-19 Limit Cycle (12° Shock Generator, $\Delta T=12K$, $p_c = 92.355kPa$) @point E $x/L=0.5$ $y/L=0.25$

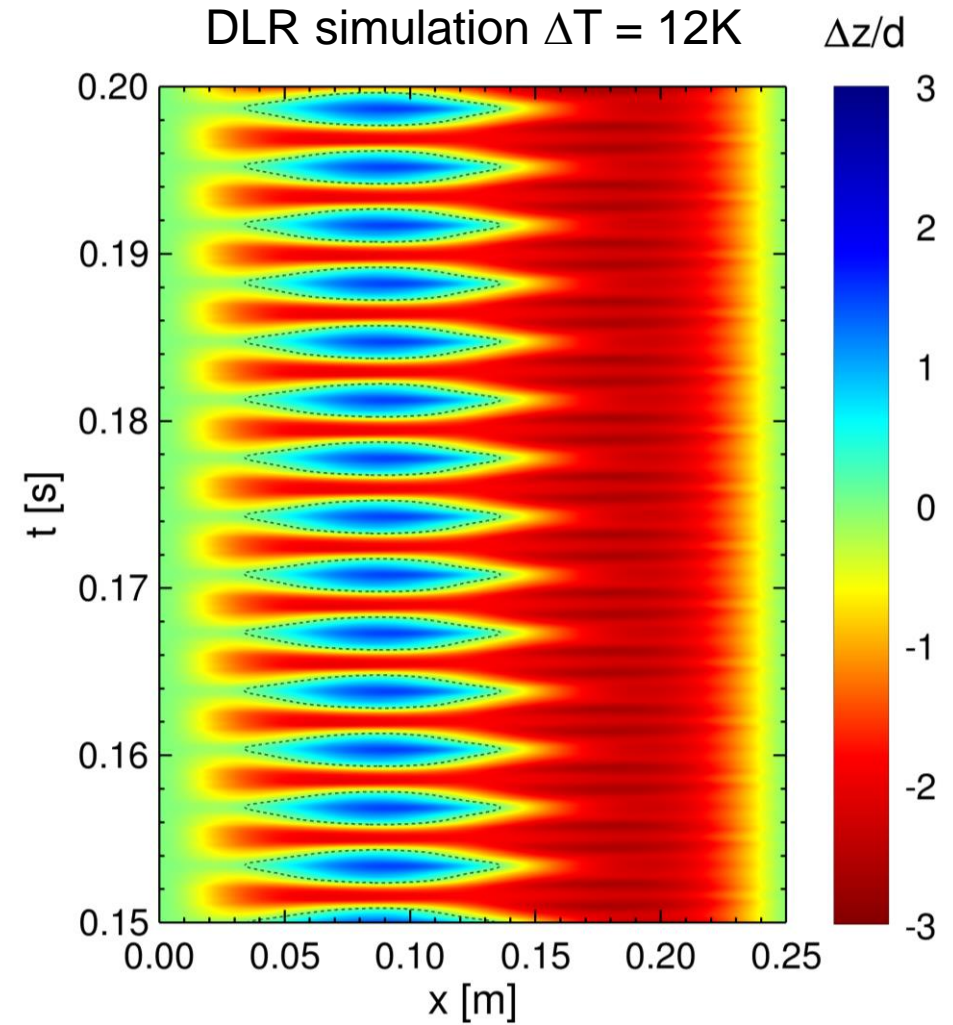
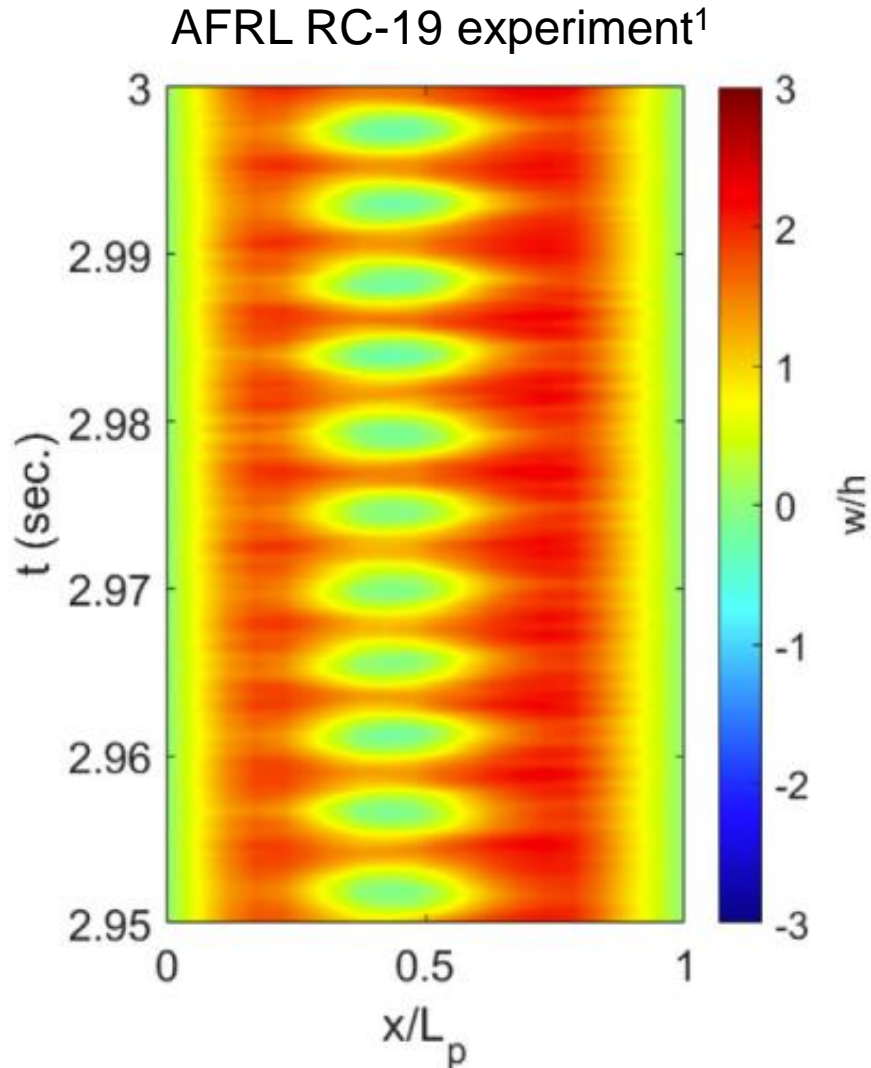


Rayleigh damping and cavity pressure



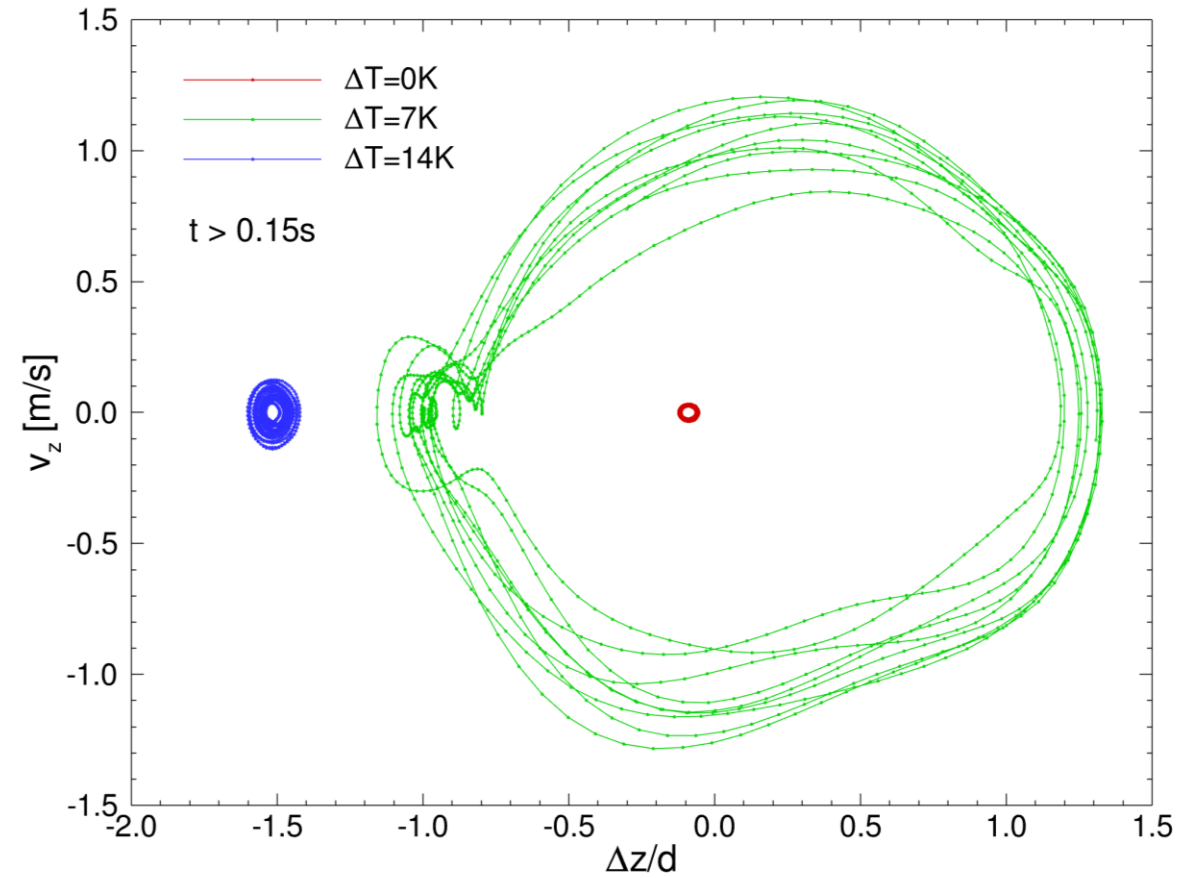
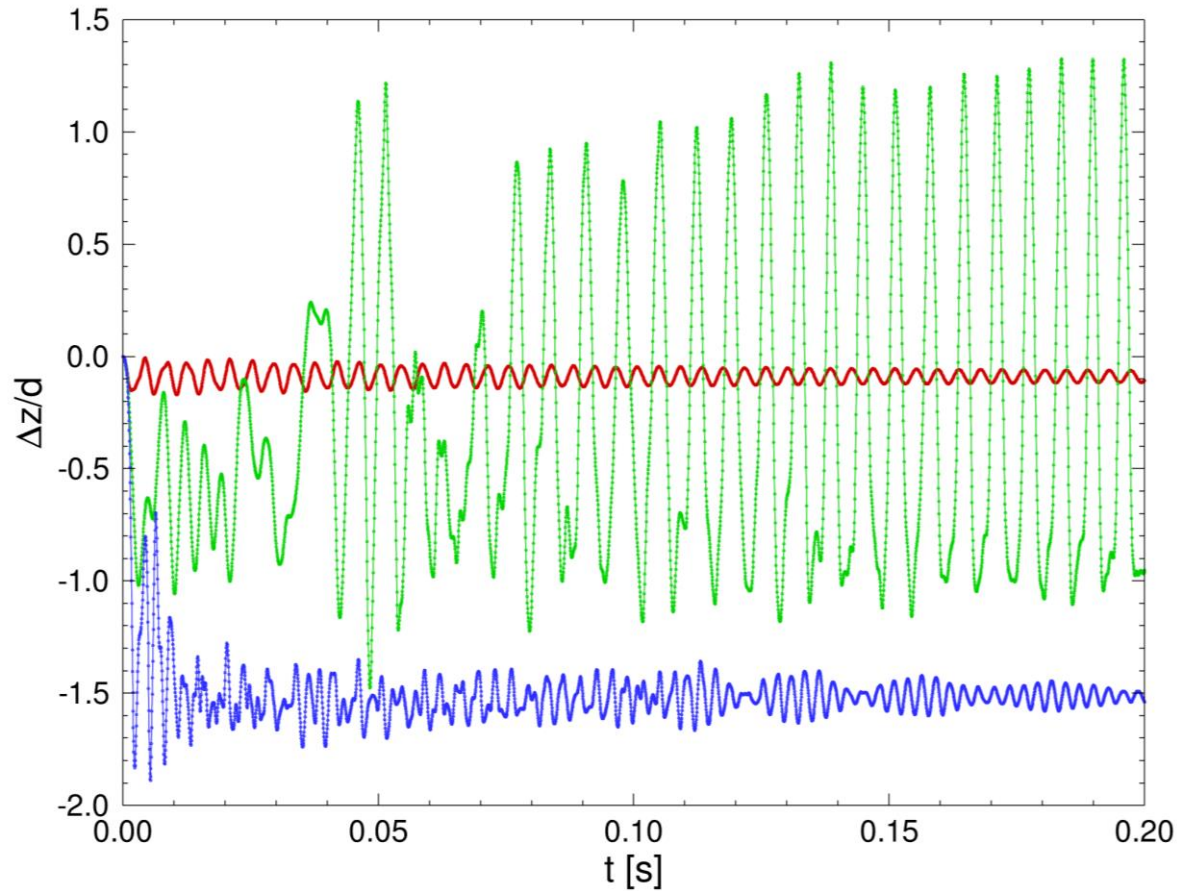
Time-history Plots

Comparison between Experiment and Simulation ($\Delta t=0.0125\text{ms}$)



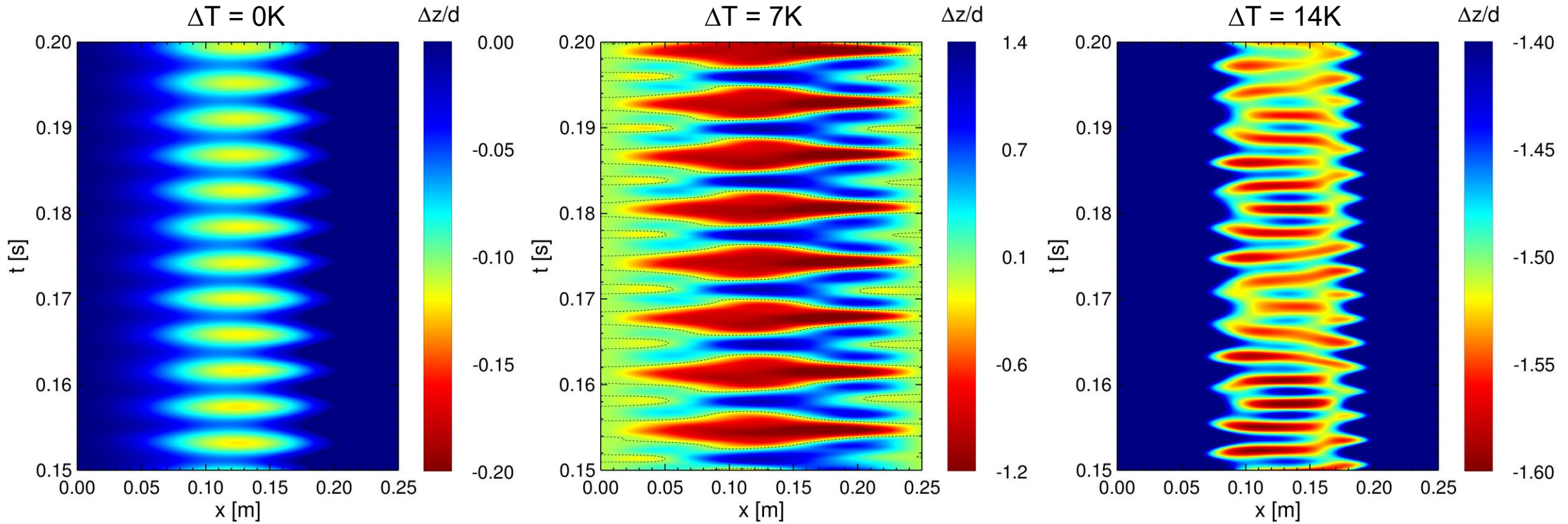
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RC-19 Panel Limit Cycle, 0° Wedge ($\Delta t = 0.05\text{ms}$, $p_c = 50.7235\text{kPa}$) @point E $x/L=0.5$ $y/L=0.25$



without structural damping and variable cavity pressure

RC-19 Panel Limit Cycle, 0° Wedge ($\Delta t = 0.05\text{ms}$, $p_c = 50.7235\text{kPa}$) @centerline $y/L=0.25$



without structural damping and variable cavity pressure

Ongoing Work and Next Steps



- Simulation of Separated SBLI ongoing
 - Cavity pressure influence
- Simulation of NoSBLI case (without wedge) periodic/chaotic transition (AePW3 test cases)
- CSM mesh possibly too fine (too many degrees of freedom) ?
- Analysis tools
 - Dynamic mode decomposition (DMD)
 - Spectral proper orthogonal decomposition (SPOD)
 - 0-1 chaos test
 - Lyapunov exponents